## Time-freezing for optimal control of systems with state jumps

#### Moritz Diehl

#### Systems Control and Optimization Laboratory Department of Microsystems Engineering and Department of Mathematics University of Freiburg, Germany

based on joint work with Armin Nurkanović, Sebastian Albrecht, Bernard Brogliato

> 9th Annual Symposium, Toulouse LAAS – CNRS, Toulouse, France 20th – 22nd September, 2022



## Nonsmooth Dynamics (NSD) - a classification

Regard ordinary differential equation (ODE) with a **nonsmooth** right-hand side (RHS). Distinguish three cases:





x(t)

NSD2: state dependent switch of RHS, e.g., 
$$\dot{x} = 2 - \operatorname{sign}(x)$$



NSD3: state dependent jump, e.g., bouncing ball,  $v(t_{+}) = -0.9 v(t_{-})$ 

# Aim of time-freezing: transform NSD3 to NSD2 (and then use the rest of the toolchain)



PSS - piecewise smooth systems; DCS - dynamic complementarity system; OCP - optimal control problem; FESD - finite elements with switch detection; MPCC - mathematical program with complementarity constraints ; NLP - nonlinear program



- ► The time-freezing reformulation
- Elastic impacts
- Inelastic impacts
- Hybrid systems with hysteresis
- Conclusions and outlook

## NSD3 state jump example: bouncing ball

Bouncing ball with state x = (q, v):

$$\begin{split} \dot{q} &= v, \, m \dot{v} = -mg, \quad \text{if} \, q > 0 \\ v(t^+) &= -0.9 \, v(t^-), \qquad \text{if} \, q(t^-) = 0 \text{ and } v(t^-) < 0 \end{split}$$

Time plot of bouncing ball trajectory:



Phase plot of bouncing ball trajectory:



Question: could we transform NSD3 systems into (easier) NSD2 systems?



- 1. mimic state jump by auxiliary dynamic system  $\dot{x} = f_{\mathrm{aux}}(x)$  on prohibited region
- 2. introduce a **clock state**  $t(\tau)$  that stops counting when the auxiliary system is active
- 3. adapt speed of time,  $\frac{dt}{d\tau} = s$  with  $s \ge 1$ , and impose terminal constraint t(T) = T

## The time-freezing reformulation

Augmented state  $(x,t) \in \mathbb{R}^{n+1}$  evolves in numerical time  $\tau$ . Augmented system is nonsmooth, of NSD2 type:

$$\frac{\mathrm{d}}{\mathrm{d}\tau} \begin{bmatrix} x \\ t \end{bmatrix} = \begin{cases} s \begin{bmatrix} f(x) \\ 1 \end{bmatrix}, & \text{ if } c(x) \ge 0 \\ \\ \begin{bmatrix} s f_{\mathrm{aux}}(x) \\ 0 \end{bmatrix}, & \text{ if } c(x) < 0 \end{cases}$$

- ► During normal times, system and clock state evolve with adapted speed s ≥ 1.
- ► Auxiliary system dx/dτ = f<sub>aux</sub>(x) mimics state jump while time is frozen, dt/dτ = 0.



#### Time-freezing for bouncing ball example



Evolution of physical time (clock state) during augmented system simulation (s = 1).



We can recover the true solution by plotting  $x(\tau)$  vs.  $t(\tau)$  and disregarding "frozen pieces".

#### Time-freezing for optimal control with state jump



 $\min_{\substack{x(.),u(.)\\\theta(.),\lambda(.)}}$ 

Regard bouncing ball in two dimensions driven by bounded force:  $\left| \, \ddot{q} = u \right.$ 



$$\begin{split} & \int_{s(.), \mu(.)}^{T} (q - q_{ref}(\tau))^{\top} (q - q_{ref}(\tau)) \, s(\tau) \, \mathrm{d}\tau \\ & \text{s.t.} \quad x(0) = x_0, \quad t(T) = T, \\ & x'(\tau) = \sum_{i=1}^{n_f} \theta_i(\tau) f_i(x(\tau), u(\tau), s(\tau)), \\ & 0 = g(x(\tau)) - \lambda(\tau) - \mu(\tau) e, \\ & 0 \leq \lambda(\tau) \perp \theta(\tau) \geq 0, \\ & 1 = e^{\top} \theta(\tau), \\ & \| u(\tau) \|_2^2 \leq u_{\max}^2, \\ & 1 \leq s(\tau) \leq s_{\max}, \ \tau \in [0, T]. \end{split}$$

$$q_{\rm ref}(\tau) = (R\cos(\omega t(\tau)), R\sin(\omega t(\tau))).$$

## Results with slowly moving reference

For  $\omega = \pi$ , tracking is easy: no jumps occur in optimal solution.



- Regard time horizon of two periods
- ▶ N = 25 equidistant control intervals
- ▶ use FESD with  $N_{\rm FE} = 3$  finite elements with Radau 3 on each control interval
- each FESD interval has one constant control u and one speed of time s
- MPCC solved via l<sub>∞</sub> penalty reformulation and homotopy
- For homotopy convergence: in total 4 NLPs solved with IPOPT via CasADi



States and controls in physical time.

#### Results with slowly moving reference - movie

For  $\omega = \pi$ , tracking is easy: no jumps occur in optimal solution.



#### Results with fast reference

For  $\omega = 2\pi$ , tracking is only possible if ball bounces against walls.





States and controls in numerical time.

States and controls in physical time.

#### Results with fast reference - movie

For  $\omega=2\pi,$  tracking is only possible if ball bounces against walls.



# Homotopy: first iteration vs converged solution

Geometric trajectory





The solution trajectory after convergence

## Physical vs. Numerical Time













- ► The time-freezing reformulation
- Elastic impacts

#### Inelastic impacts

- Hybrid systems with hysteresis
- Conclusions and outlook

Complementarity Lagrangian Systems (CLS)

$$\begin{split} \dot{q} &= v, \\ M(q) \dot{v} &= \tilde{f}_{v}(q, v, u) + \nabla_{q} f_{c}(q) \lambda_{n} + B(q) \lambda_{t}, \\ 0 &\leq \lambda_{n} \perp f_{c}(q) \geq 0, \\ 0 &= n(q(t_{s}))^{\top} v(t_{s}^{+}), \text{ if } f_{c}(q(t_{s})) = 0 \text{ and } n(q(t_{s}))^{\top} v(t_{s}^{-}) < 0, \\ \lambda_{t} &\in \arg \min_{\tilde{\lambda}_{t} \in \mathbb{R}^{n_{t}}} -v^{\top} B(q) \tilde{\lambda}_{t} \\ \text{ s.t. } \|\tilde{\lambda}_{t}\|_{2} \leq \mu \lambda_{n}. \end{split}$$

- ▶ we regard a single unilateral constraint  $f_c(q) \ge 0$
- ▶  $n(q) := \nabla_q f_c(q)$  is the normal vector of the contact manifold  $\{q \in \mathbb{R}^{n_q} \mid f_c(q) = 0\}$
- $\blacktriangleright~B(q)\in \mathbb{R}^{n_q\times n_t}$  ,  $n_{\rm t}=n_q-1$  spans the tangent plane
- For a moment let us ignore tangential friction (red terms)

Complementarity Lagrangian Systems (CLS)

$$\begin{split} \dot{q} &= v, \\ M(q)\dot{v} &= \tilde{f}_{v}(q, v, u) + \nabla_{q}f_{c}(q)\lambda_{n} \\ 0 &\leq \lambda_{n} \perp f_{c}(q) \geq 0, \\ 0 &= n(q(t_{s}))^{\top}v(t_{s}^{+}), \text{ if } f_{c}(q(t_{s})) = 0 \text{ and } n(q(t_{s}))^{\top}v(t_{s}^{-}) < 0, \end{split}$$

• we regard a single unilateral constraint  $f_c(q) \ge 0$ 

▶  $n(q) := \nabla_q f_c(q)$  is the normal vector of the contact manifold  $\{q \in \mathbb{R}^{n_q} \mid f_c(q) = 0\}$ 

For a moment let us ignore tangential friction

#### Notation and basic definitions

CLS modes and contact LCP



#### unconstrained ODE mode

$$\dot{q} = v,$$
  
$$\dot{v} = \underbrace{M(q)^{-1}\tilde{f}_{v}(q, v, u)}_{=:f_{v}(q, v, u)},$$

#### contact mode - DAE of index 3

$$\begin{split} \dot{q} &= v \\ \dot{v} &= M(q)^{-1} \left( \tilde{f}_{\rm v}(q,v,u) + \nabla_q f_c(q) \lambda_{\rm n} \right), \\ 0 &= f_c(q). \end{split}$$

#### Notation and basic definitions

CLS modes and contact LCP



#### unconstrained ODE mode

$$\dot{q} = v,$$
  
$$\dot{v} = \underbrace{M(q)^{-1}\tilde{f}_{v}(q, v, u)}_{=:f_{v}(q, v, u)},$$

contact mode - DAE of index 3  $\dot{q} = v$   $\dot{v} = M(q)^{-1} \left( \tilde{f}_{v}(q, v, u) + \nabla_{q} f_{c}(q) \lambda_{n} \right),$  $0 = f_{c}(q).$ 

The contact LCP tells us if the system will stay in contact mode or switch to the ODE mode:

$$\begin{split} 0 &\leq \frac{\mathrm{d}^2}{\mathrm{d}t^2} f_c(q(t)) \perp \lambda_{\mathrm{n}}(t) \geq 0 \iff \\ 0 &\leq D(q)\lambda_{\mathrm{n}} + \varphi(x) \perp \lambda_{\mathrm{n}} \geq 0, \text{ solution:} \quad \lambda_{\mathrm{n}} = \max(0, -D(q)^{-1}\varphi(x)) \end{split}$$

#### Notation and basic definitions

CLS modes and contact LCP



#### unconstrained ODE mode

$$\dot{q} = v,$$
  
$$\dot{v} = \underbrace{M(q)^{-1} \tilde{f}_{v}(q, v, u)}_{=:f_{v}(q, v, u)},$$

contact mode - DAE of index 3  $\dot{q} = v$   $\dot{v} = M(q)^{-1} \left( \tilde{f}_{v}(q, v, u) + \nabla_{q} f_{c}(q) \lambda_{n} \right),$  $0 = f_{c}(q).$ 

The contact LCP tells us if the system will stay in contact mode or switch to the ODE mode:

$$\begin{split} 0 &\leq \frac{\mathrm{d}^2}{\mathrm{d}t^2} f_c(q(t)) \perp \lambda_{\mathrm{n}}(t) \geq 0 \iff \\ 0 &\leq D(q)\lambda_{\mathrm{n}} + \varphi(x) \perp \lambda_{\mathrm{n}} \geq 0, \text{ solution:} \quad \lambda_{\mathrm{n}} = \max(0, -D(q)^{-1}\varphi(x)) \end{split}$$

where D(q) is the Delassus' matrix (scalar in this case) and

$$D(q) \coloneqq \nabla_q f_c(q)^\top M(q)^{-1} \nabla_q f_c(q) \succ 0, \quad \varphi(x) \coloneqq \nabla_q f_c(q)^\top f_v(q, v, u) + \nabla_q (\nabla_q f_c(q)^\top v)^\top v.$$



Trajectory with u(t) = 0:





## Warm up example

Phase plots: elastic vs. inelastic impact





## Time-freezing for inelastic impacts

Back to the more general setting



State space in numerical time 
$$\tau$$
:  $y = (q, v, t) \in \mathbb{R}^{n_y}, n_y = n_x + 1$  and  $x = (q, v)$ 

Switching functions  

$$c_1(y) := f_c(q)$$

$$c_2(y) := \nabla_q f_c(q)^\top \quad \left(= \frac{\mathrm{d}f_c}{\mathrm{d}t}(q)\right)$$

#### Regions

$$\begin{split} R_1^a &= \{ y \in \mathbb{R}^{n_y} \mid c_1(y) > 0 \} \\ R_1^b &= \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) > 0 \} \\ R_1 &= R_1^a \cup R_2^b \\ R_2 &= \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \} \end{split}$$



- R<sub>1</sub> unconstrained dynamics
- R<sub>2</sub> auxiliary dynamics
- After impact:  $c_1(y) = c_2(y) = 0$
- ► sliding mode on  $\Sigma = \{y \mid c_1(y) = 0, c_2(y) = 0\}$

## Time-freezing for inelastic impacts

Back to the more general setting

• State space in numerical time 
$$au\colon y=(q,v,t)\in\mathbb{R}^{n_y},\ n_y=n_x+1$$
 and  $x=(q,v)$ 

Switching functions  

$$c_1(y) := f_c(q)$$

$$c_2(y) := \nabla_q f_c(q)^\top \quad \left( = \frac{\mathrm{d}f_c}{\mathrm{d}t}(q) \right)$$

#### Regions

$$\begin{split} R_1^a &= \{ y \in \mathbb{R}^{n_y} \mid c_1(y) > 0 \} \\ R_1^b &= \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) > 0 \} \\ R_1 &= R_1^a \cup R_2^b \\ R_2 &= \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \} \end{split}$$



- R<sub>1</sub> unconstrained dynamics
- R<sub>2</sub> auxiliary dynamics
- After impact:  $c_1(y) = c_2(y) = 0$
- ► sliding mode on  $\Sigma = \{y \mid c_1(y) = 0, c_2(y) = 0\}$

## Unconstrained and auxiliary dynamics

#### Unconstrained free-flight ODE in $R_1$

$$y' = f_{\text{ODE}}(y, u) \coloneqq \begin{bmatrix} v \\ f_{v}(q, v, u) \\ 1 \end{bmatrix}$$

Auxiliary ODE in  $R_2$ 

$$y'(\tau) = f_{\text{aux},n}(y) \coloneqq \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1}n(q)a_n \\ \mathbf{0} \end{bmatrix}$$

with  $a_n > 0$ .



## Unconstrained and auxiliary dynamics

#### Unconstrained free-flight ODE in $R_1$

$$y' = f_{\text{ODE}}(y, u) \coloneqq \begin{bmatrix} v \\ f_v(q, v, u) \\ 1 \end{bmatrix}$$

Auxiliary ODE in  $R_2$ 

$$y'(\tau) = f_{\text{aux},n}(y) \coloneqq \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1}n(q)a_n \\ \mathbf{0} \end{bmatrix}$$

with  $a_n > 0$ .



## Unconstrained and auxiliary dynamics

#### Unconstrained free-flight ODE in $R_1$

$$y' = f_{\text{ODE}}(y, u) \coloneqq \begin{bmatrix} v \\ f_v(q, v, u) \\ 1 \end{bmatrix}$$

Auxiliary ODE in  $R_2$ 

$$y'(\tau) = f_{\text{aux},\mathbf{n}}(y) \coloneqq \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1}n(q)a_{\mathbf{n}} \\ \mathbf{0} \end{bmatrix}$$

with  $a_n > 0$ .



## Contact breaking

The contact LCP function  $\varphi(x)$  tells us about the vector field in  $R_1$ 

- $\varphi(x)$  determines stability of  $\Sigma$  (remember the contact LCP)
- staying in sliding mode (persistent contact) or leaving sliding mode (contact breaking) is possible



Sliding mode if  $\varphi(x) \leq 0$ 



## Contact breaking

The contact LCP function  $\varphi(x)$  tells us about the vector field in  $R_1$ 

- $\varphi(x)$  determines stability of  $\Sigma$  (remember the contact LCP)
- staying in sliding mode (persistent contact) or leaving sliding mode (contact breaking) is possible



Breaking contact if  $\varphi(x) > 0$ 

Sliding mode if  $\varphi(x) \leq 0$ 

Moritz Diehl












Warm up example: a linearly increasing vertical force beats gravity



#### Time-freezing system

$$y' \in F_{\mathrm{TF}}(y, u) = \{\theta_1 f_{\mathrm{ODE}}(y, u) + \theta_2 f_{\mathrm{aux}, n}(y) \mid \theta^\top e = 1, \ \theta \ge 0\}$$

- fractional  $\theta_1, \theta_2 \in (0, 1)$  ensures sliding on  $\Sigma$
- ▶ speed of time  $\frac{\mathrm{d}t}{\mathrm{d}\tau} = \theta_1 \cdot 1 + \theta_2 \cdot 0 < 1$  slow down
- resulting dynamics equal to reduced DAE index 3 dynamics f<sub>DAE</sub>(x, u) (contact mode)
- auxiliary dynamics plays role of contact force (keeps v = 0 and avoids penetration)



#### The sliding mode is unique

#### Time-freezing system

$$y' \in F_{\rm TF}(y, u) = \{\theta_1 f_{\rm ODE}(y, u) + \theta_2 f_{{\rm aux}, n}(y) \mid \theta^\top e = 1, \ \theta \ge 0\}$$
 (1)

#### Theorem

Let  $y(\tau)$  be a solution of the dyn. system (1) with  $y(0) \in \Sigma = \{y \in \mathbb{R}^{n_y} \mid c_1(y) = 0, c_2(y) = 0\}$  and  $\tau \in [0, \tau_f]$ . Suppose that  $\varphi(x(\tau), u(\tau)) \leq 0$  for all  $\tau \in [0, \tau_f]$  (persistent contact), then the following statements are true:

- (i) the convex multipliers  $\theta_1, \theta_2 \ge 0$  are unique,
- (ii) the dynamics of the sliding mode are given by  $y' = \gamma(x, u) \begin{vmatrix} f_{\text{DAE}}(x, u) \\ 1 \end{vmatrix}$ , where

 $\gamma(x,u)\in(0,1]$  is a time-rescaling factor given by

$$\gamma(x,u) \coloneqq \frac{D(q)a_{n}}{D(q)a_{n} - \varphi(x,u)}.$$
(2)



# Time-freezing with friction

Complementarity Lagrangian Systems (CLS)

$$\begin{split} \dot{q} &= v, \\ M(q)\dot{v} &= \tilde{f}_{v}(q, v, u) + \nabla_{q}f_{c}(q)\lambda_{n} + B(q)\lambda_{t}, \\ 0 &\leq \lambda_{n} \perp f_{c}(q) \geq 0, \\ 0 &= n(q(t_{s}))^{\top}v(t_{s}^{+}), \text{ if } f_{c}(q(t_{s})) = 0 \text{ and } n(q(t_{s}))^{\top}v(t_{s}^{-}) < 0, \\ \lambda_{t} &\in \arg\min_{\tilde{\lambda}_{t} \in \mathbb{R}^{n_{t}}} -v^{\top}B(q)\tilde{\lambda}_{t} \\ \text{ s.t. } \|\tilde{\lambda}_{t}\|_{2} \leq \mu\lambda_{n}. \end{split}$$

• we regard  $f_c(x) \in \mathbb{R}$  (single unilateral constraint)

- ▶  $B(q) \in \mathbb{R}^{n_q \times n_t}$  spans the tangent plane at contact points  $C(q) := \{q \in \mathbb{R}^{n_q} \mid f_c(q) = 0\}$ ,  $n_t \in \{1, 2\}$ , tang. velocity  $v_t = B(q)v$
- ▶ We derive time-freezing for the red terms

## Coulomb's friction

Solution map for a given  $\lambda_n$ 



#### Coulomb's friction law

$$egin{aligned} &\lambda_{\mathrm{t}} \in \arg\min_{ ilde{\lambda}_{\mathrm{t}} \in \mathbb{R}^{n_{\mathrm{t}}}} & -v_{\mathrm{t}}^{ op} ilde{\lambda}_{\mathrm{t}} \ &\mathrm{s.t.} & \| ilde{\lambda}_{\mathrm{t}}\|_{2} \leq \mu\lambda_{\mathrm{n}}. \end{aligned}$$

#### Friction solution map

$$\lambda_{\mathbf{t}} \in \begin{cases} \{-\mu\lambda_{\mathbf{n}}\frac{v_{\mathbf{t}}}{\|v_{\mathbf{t}}\|_{2}}\}, & \text{if } \|v_{\mathbf{t}}\|_{2} > 0, \\ \{\tilde{\lambda}_{\mathbf{t}} \mid \|\tilde{\lambda}_{\mathbf{t}}\|_{2} \le \mu\lambda_{\mathbf{n}}\}, & \text{if } \|v_{\mathbf{t}}\|_{2} = 0. \end{cases}$$

## Coulomb's friction

Solution map for a given  $\lambda_n$ 



#### Coulomb's friction law

$$\begin{split} \lambda_{\mathbf{t}} &\in \arg\min_{\tilde{\lambda}_{\mathbf{t}} \in \mathbb{R}^{n_{\mathbf{t}}}} \quad -v_{\mathbf{t}}^{\top} \tilde{\lambda}_{\mathbf{t}} \\ \text{s.t.} \quad \|\tilde{\lambda}_{\mathbf{t}}\|_{2} \leq \mu \lambda_{\mathbf{n}}. \end{split}$$

#### Friction solution map

$$\lambda_{\mathbf{t}} \in \begin{cases} \{-\mu\lambda_{\mathbf{n}} \frac{v_{\mathbf{t}}}{\|v_{\mathbf{t}}\|_{2}}\}, & \text{if } \|v_{\mathbf{t}}\|_{2} > 0, \\ \{\tilde{\lambda}_{\mathbf{t}} \mid \|\tilde{\lambda}_{\mathbf{t}}\|_{2} \le \mu\lambda_{\mathbf{n}}\}, & \text{if } \|v_{\mathbf{t}}\|_{2} = 0. \end{cases}$$

▶ reduces to  $\lambda_t \in -\lambda_n sign(v_t)$  in planar case

- ▶ the normal impulse is  $a_n \tau_{jump} \implies$  the tangential impulse should be  $-\mu a_n \tau_{jump} \operatorname{sign}(v_t)$
- trivially, tangential impulse happens at same time as the normal impulse
- ▶ **Conclusion**: make aux. dyn. in tangential directions B(q) "proportional" to  $f_{\text{aux,n}}$  and let them evolve simultaneously

Refine the definitions for  $c_1(y) < 0$  and  $c_2(y) < 0$  to account for the sign of  $v_{\rm t}$ 

New additional switching function  $c_3(y) = v_t$ 

#### Regions

$$Q = \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \}$$
  

$$R_1 = R_1^a \cup R_1^b$$
  

$$R_2 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) > 0 \}$$
  

$$R_3 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) < 0 \}$$



$$y' \in F_{\rm TF}(y, u) = \left\{ \sum_{i=1}^{3} f_i(y, u) \mid \theta \ge 0, \ e^{\top} \theta = 1 \right\}$$
 (3)

Refine the definitions for  $c_1(y) < 0$  and  $c_2(y) < 0$  to account for the sign of  $v_{\rm t}$ 

New additional switching function  $c_3(y) = v_t$ 

#### Regions

$$Q = \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \}$$
  

$$R_1 = R_1^a \cup R_1^b$$
  

$$R_2 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) > 0 \}$$
  

$$R_3 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) < 0 \}$$



$$y' \in F_{\rm TF}(y, u) = \left\{ \sum_{i=1}^{3} f_i(y, u) \mid \theta \ge 0, \ e^{\top} \theta = 1 \right\}$$
 (3)

Refine the definitions for  $c_1(y) < 0$  and  $c_2(y) < 0$  to account for the sign of  $v_{\rm t}$ 

New additional switching function  $c_3(y) = v_t$ 

#### Regions

$$Q = \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \}$$
  

$$R_1 = R_1^a \cup R_1^b$$
  

$$R_2 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) > 0 \}$$
  

$$R_3 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) < 0 \}$$



$$y' \in F_{\rm TF}(y, u) = \left\{ \sum_{i=1}^{3} f_i(y, u) \mid \theta \ge 0, \ e^{\top} \theta = 1 \right\}$$
 (3)

Refine the definitions for  $c_1(y) < 0$  and  $c_2(y) < 0$  to account for the sign of  $v_{\rm t}$ 

New additional switching function  $c_3(y) = v_t$ 

#### Regions

$$Q = \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \}$$
  

$$R_1 = R_1^a \cup R_1^b$$
  

$$R_2 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) > 0 \}$$
  

$$R_3 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) < 0 \}$$



$$y' \in F_{\rm TF}(y,u) = \left\{ \sum_{i=1}^{3} f_i(y,u) \mid \theta \ge 0, \ e^{\top}\theta = 1 \right\}$$
 (3)

Refine the definitions for  $c_1(y) < 0$  and  $c_2(y) < 0$  to account for the sign of  $v_t$ 

New additional switching function  $c_3(y) = v_t$ 

#### Regions

$$Q = \{ y \in \mathbb{R}^{n_y} \mid c_1(y) < 0, c_2(y) < 0 \}$$
  

$$R_1 = R_1^a \cup R_1^b$$
  

$$R_2 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) > 0 \}$$
  

$$R_3 = Q \cap \{ y \in \mathbb{R}^{n_y} \mid c_3(y) < 0 \}$$



$$y' \in F_{\rm TF}(y, u) = \left\{ \sum_{i=1}^{3} f_i(y, u) \mid \theta \ge 0, \ e^{\top} \theta = 1 \right\}$$
(3)

## Time-freezing with friction in the planar case



#### PSS modes

$$\begin{split} f_1(y,u) &= (f_{\text{ODE}}(x,u),1) \\ f_2(y) &= f_{\text{aux},n}(y) - f_{\text{aux},t}(y) \\ f_3(y) &= f_{\text{aux},n}(y) + f_{\text{aux},t}(y) \end{split}$$

#### Auxiliary ODE for tangential directions

$$f_{\text{aux,t}}(y) \coloneqq \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1} \mathbf{B}(q) \mu \ a_n \\ \mathbf{0} \end{bmatrix}$$
$$f_{\text{aux,n}}(y) \coloneqq \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1} n(q) a_n \\ \mathbf{0} \end{bmatrix}$$

Simply sum the auxiliary dynamics in normal and tangential directions (recall that  $B(q) \in \mathbb{R}^{n_q \times 1}$  and  $n(q) \perp B(q)$ )

State jump is over when  $n(q)^{\top}v = 0$ , friction to slow down

 $\blacktriangleright \text{ With } v_t = 0 \text{ sliding mode on } \Gamma = \{y \mid c_1(y) = 0, c_2(y) = 0, c_3(y) = 0\}$ 

## Time-freezing with friction - sliding mode dynamics

• 
$$\dot{x} = f_{Slip}(x, u)$$
 reduced DAE in slip mode,  $v_t \neq 0$ 

•  $\dot{x} = f_{\mathrm{Stick}}(x, u)$  reduced DAE in stick mode,  $v_{\mathrm{t}} = 0$ 

#### Theorem (Slip-stick sliding mode)

Let  $y(\tau)$  be a solution of time freezing system (3) with  $y(0) \in \Sigma$  and  $\tau \in [0, \tau_f]$ . Suppose that  $\varphi(x(\tau), u(\tau)) \leq 0$  for all  $\tau \in [0, \tau_f]$  (persistent contact), then the following statements are true:

Increasing  $\mu = 0$  to  $\mu = 0.5$  with  $\Delta \mu = 0.1$ .



External force  $u_x = 2$  $\mu = 0$ No friction



Increasing  $\mu = 0$  to  $\mu = 0.5$  with  $\Delta \mu = 0.1$ .



 $\begin{array}{l} \mbox{External force } u_x = 2 \\ \mu = 0.1 \\ \mbox{External force stronger than friction} \end{array}$ 



Increasing  $\mu = 0$  to  $\mu = 0.5$  with  $\Delta \mu = 0.1$ .



External force  $u_x = 2$  $\mu = 0.2$ External force equal to friction



Increasing  $\mu = 0$  to  $\mu = 0.5$  with  $\Delta \mu = 0.1$ .



External force  $u_x=2$   $\mu=0.3$  External force weaker than friction



Increasing  $\mu = 0$  to  $\mu = 0.5$  with  $\Delta \mu = 0.1$ .



External force  $u_x=2$   $\mu=0.4$  External force weaker than friction



Increasing  $\mu = 0$  to  $\mu = 0.5$  with  $\Delta \mu = 0.1$ .



External force  $u_x=2$   $\mu=0.5$  Tangential velocity zero after impact



## Friction for 3D contacts

#### Friction solution map

$$\lambda_{\mathbf{t}} \in \begin{cases} \{-\mu\lambda_{\mathbf{n}} \frac{v_{\mathbf{t}}}{\|v_{\mathbf{t}}\|_{2}}\}, & \text{if } \|v_{\mathbf{t}}\|_{2} > 0, \\ \{\tilde{\lambda}_{\mathbf{t}} \mid \|\tilde{\lambda}_{\mathbf{t}}\|_{2} \le \mu\lambda_{\mathbf{n}}\}, & \text{if } \|v_{\mathbf{t}}\|_{2} = 0. \end{cases}$$

- ▶ The set  $\{v_t \mid v_t = 0\}$  has an empty interior
- Problematic for defining Filippov system
   via θ multipliers
- Problem not present with polyhedral approximations



#### Relaxed riction solution map

$$\lambda_{t} = \begin{cases} -\mu \lambda_{n} \frac{v_{t}}{\|v_{t}\|_{2}}, & \text{if } \|v_{t}\|_{2} > \epsilon_{t}, \\ v_{t}, & \text{if } \|v_{t}\|_{2} < \epsilon_{t}, \end{cases}$$

- $\epsilon_t > 0$  can be arbitrarily small
- Obtain set with nonempty interior
- Slip mode: approximation is exact
- Stick mode: sliding mode on  $||v_t||_2 = \epsilon_t$
- Approximation can be made arbitrarily good



## Friction for 3D contacts - the time-freezing system

Time-freezing system with friction

$$y' \in F_{\rm TF}(y, u) = \left\{ \sum_{i=1}^{3} f_i(y, u) \mid \theta \ge 0, \ e^{\top} \theta = 1 \right\}$$

#### PSS modes

$$\begin{split} f_1(y, u) &= (f_{\text{ODE}}(x, u), 1) \\ f_2(y) &= f_{\text{aux}, n}(y) - f_{\text{aux}, t, 2}(y) \\ f_3(y) &= f_{\text{aux}, n}(y) + f_{\text{aux}, t, 3}(y) \end{split}$$

- ► Use same definition of regions R<sub>1</sub>, R<sub>2</sub> and R<sub>3</sub>
- Switching function  $c_3(y) = \|v_t\|_2 \epsilon_t$

#### Auxiliary ODEs for 3D friction

$$f_{\text{aux,t,2}}(y) = \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1} B(q) \mu a_n \frac{v_t}{\|v_t\|} \\ 0 \end{bmatrix}$$
$$f_{\text{aux,t,3}}(y) = \begin{bmatrix} \mathbf{0}_{n_q,1} \\ M(q)^{-1} B(q) v_t \\ 0 \end{bmatrix}$$

## Hopping robot - move with minimal effort from start to end position

Homotopy initialized with start position everywhere. Optimizer finds creative solution.



- ► The time-freezing reformulation
- ► Elastic impacts
- Inelastic impacts
- Hybrid systems with hysteresis
- Conclusions and outlook

## Hybrid systems and finite automaton





### Hybrid systems and finite automaton



#### Hybrid system with hysteresis (incomplete description)

$$\dot{x} = f(x, w) = (1 - w)f_{\rm A}(x) + wf_{\rm B}(x)$$

### Tutorial example: thermostat with hysteresis





## Tutorial example: thermostat with hysteresis



## Hysteresis: a system with state jumps



### Hysteresis: a system with state jumps



#### The State Jump Law

1. if 
$$w(t_s^-) = 0$$
 and  $\psi(x(t_s^-)) = 1$ , then  $x(t_s^+) = x(t_s^-)$  and  $w(t_s^+) = 1$ 

2. if 
$$w(t_{
m s}^-)=1$$
 and  $\psi(x(t_{
m s}^-))=0$ , then  $x(t_{
m s}^+)=x(t_{
m s}^-)$  and  $w(t_{
m s}^+)=0$ 

**Remember**: w(t) is now a discontinuous differential state!



- 1. mimic state jump by auxiliary dynamical system on prohibited region
- 2. introduce a **clock state**  $t(\tau)$  that stops counting when the auxiliary system is active



- 1. mimic state jump by auxiliary dynamical system on prohibited region
- 2. introduce a **clock state**  $t(\tau)$  that stops counting when the auxiliary system is active
- 3. time-freezing system (a PSS) evolves in numerical time  $\tau$ , initial system (with state jumps) in physical time  $t(\tau)$
- 4. adapt speed of time,  $\frac{dt}{d\tau} = s$  with  $s \ge 1$ , and impose terminal constraint t(T) = T



- 1. mimic state jump by auxiliary dynamical system on prohibited region
- 2. introduce a **clock state**  $t(\tau)$  that stops counting when the auxiliary system is active
- 3. time-freezing system (a PSS) evolves in numerical time  $\tau$ , initial system (with state jumps) in physical time  $t(\tau)$
- 4. adapt speed of time,  $\frac{dt}{d\tau} = s$  with  $s \ge 1$ , and impose terminal constraint t(T) = T
- 5. if the state dimension reduces after a state jump, construct an appropriate sliding mode



- 1. mimic state jump by auxiliary dynamical system on prohibited region
- 2. introduce a clock state  $t(\tau)$  that stops counting when the auxiliary system is active
- 3. time-freezing system (a PSS) evolves in numerical time  $\tau$ , initial system (with state jumps) in physical time  $t(\tau)$
- 4. adapt speed of time,  $\frac{dt}{d\tau} = s$  with  $s \ge 1$ , and impose terminal constraint t(T) = T
- 5. if the state dimension reduces after a state jump, construct an appropriate sliding mode 6. take  $x(t(\tau))$  instead of  $x(\tau)$  to recover the original solution with state jumps
- 7. ...

## Tutorial example: thermostat and time-freezing


# Time-freezing: the state space

A look at the  $(\psi(x),w)-{\rm plane}$ 



- Everything except the blue solid curve is prohibited in the  $(\psi, w)$  space (use 1<sup>st</sup> principle of time-freezing)
- ► The evolution happens in a lower-dimensional space ⇒ sliding mode (use 4<sup>th</sup> principle of time-freezing)

# Time-freezing: partitioning of the space

An efficient partition leads to less variables in FESD



Partition the state space into Voronoi regions:  $R_i = \{z \mid ||z - z_i||^2 < ||z - z_j||^2, \ j = 1, \dots, 4, j \neq i\}, \ z = (\psi(x), w)$ 

# Time-freezing: partitioning of the space

An efficient partition leads to less variables in FESD



Partition the state space into Voronoi regions:  $R_i = \{z \mid ||z - z_i||^2 < ||z - z_j||^2, j = 1, \dots, 4, j \neq i\}, z = (\psi(x), w)$ 

▶ Feasible region for initial hybrid system with hysteresis on the region boundaries

To mimic state jumps in finite numerical time



 $\blacktriangleright$  Use regions  $R_2$  and  $R_3$  to define auxiliary dynamics for the state jumps of  $w(\cdot)$ 



To mimic state jumps in finite numerical time



 $\blacktriangleright$  Use regions  $R_2$  and  $R_3$  to define auxiliary dynamics for the state jumps of  $w(\cdot)$ 

• Evolution in w-direction happens only for  $\psi \in \{0, 1\}$ 



To mimic state jumps in finite numerical time





- Use regions  $R_2$  and  $R_3$  to define auxiliary dynamics for the state jumps of  $w(\cdot)$
- Evolution in w-direction happens only for  $\psi \in \{0, 1\}$
- Zoom in: with a naive approach one has locally nonunique solutions



The new state space of the system is  $y=(x,w,t)\in \mathbb{R}^{n_x+2}$ 

#### Auxiliary dynamics

$$\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{aux,A}}(y) \coloneqq \begin{bmatrix} 0\\ -\gamma(\psi(x))\\ 0 \end{bmatrix}$$
$$\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{aux,B}}(y) \coloneqq \begin{bmatrix} 0\\ \gamma(\psi(x) - 1)\\ 0 \end{bmatrix}$$
$$y(x) = \frac{ax^2}{1 + x^2}$$



Moritz Diehl





Smart choice of auxiliary dynamics resolves the nonuniqueness issue





- Smart choice of auxiliary dynamics resolves the nonuniqueness issue
- Zoom in: escape only in one direction possible

# Time-freezing: DAE forming dynamics

Stop the state jump and construct suitable sliding mode





**b** Dynamics in  $R_1$  and  $R_4$  stops evolution of auxiliary ODE - similar to inelastic impacts

# Time-freezing: DAE forming dynamics

Stop the state jump and construct suitable sliding mode



Dynamics in R<sub>1</sub> and R<sub>4</sub> stops evolution of auxiliary ODE - similar to inelastic impacts
 Sliding modes on R<sub>A</sub> := ∂R<sub>1</sub> ∩ ∂R<sub>2</sub> and R<sub>B</sub> := ∂R<sub>3</sub> ∩ ∂R<sub>4</sub> match f<sub>A</sub>(y) and f<sub>B</sub>(y), resp.



#### DAE-forming dynamics

y = (x, w, t)  $\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{df}, \mathrm{A}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{A}}(x) \\ \gamma(\psi(x)) \\ 2 \end{bmatrix}$   $\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{df}, \mathrm{B}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{B}}(x) \\ -\gamma(\psi(x) - 1) \\ 2 \end{bmatrix}$ 

In total four regions  $R_i$ , i = 1, 2, 3, 4 and evolution of original system is the **sliding mode** 



#### DAE-forming dynamics

$$\begin{split} y &= (x, w, t) \\ \frac{\mathrm{d}y}{\mathrm{d}\tau} &= f_{\mathrm{df}, \mathrm{A}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{A}}(x) \\ \gamma(\psi(x)) \\ 2 \end{bmatrix} \\ \frac{\mathrm{d}y}{\mathrm{d}\tau} &= f_{\mathrm{df}, \mathrm{B}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{B}}(x) \\ -\gamma(\psi(x) - 1) \\ 2 \end{bmatrix} \end{split}$$

- In total four regions R<sub>i</sub>, i = 1, 2, 3, 4 and evolution of original system is the sliding mode
- ▶ Regions R<sub>2</sub> and R<sub>3</sub> equipped with aux. dynamics y' = f<sub>2</sub>(y) = f<sub>aux,A</sub>(y) and y' = f<sub>3</sub>(y) = f<sub>aux,B</sub>(y), resp., to mimic state jump



#### DAE-forming dynamics

$$y = (x, w, t)$$

$$\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{df}, \mathrm{A}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{A}}(x) \\ \gamma(\psi(x)) \\ 2 \end{bmatrix}$$

$$\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{df}, \mathrm{B}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{B}}(x) \\ -\gamma(\psi(x) - 1) \\ 2 \end{bmatrix}$$

- In total four regions R<sub>i</sub>, i = 1, 2, 3, 4 and evolution of original system is the sliding mode
- ▶ Regions  $R_2$  and  $R_3$  equipped with aux. dynamics  $y' = f_2(y) = f_{aux,A}(y)$  and  $y' = f_3(y) = f_{aux,B}(y)$ , resp., to mimic state jump
- Regions R<sub>1</sub> and R<sub>4</sub> equipped with DAE-forming dynamics y' = f<sub>1</sub>(y) = f<sub>df,A</sub>(y) and y' = f<sub>4</sub>(y) = f<sub>df,B</sub>(y), resp., to recover original dynamics in sliding mode



#### DAE-forming dynamics

$$y = (x, w, t)$$

$$\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{df,A}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{A}}(x) \\ \gamma(\psi(x)) \\ 2 \end{bmatrix}$$

$$\frac{\mathrm{d}y}{\mathrm{d}\tau} = f_{\mathrm{df,B}}(y) \coloneqq \begin{bmatrix} 2f_{\mathrm{B}}(x) \\ -\gamma(\psi(x) - 1) \\ 2 \end{bmatrix}$$

- In total four regions R<sub>i</sub>, i = 1, 2, 3, 4 and evolution of original system is the sliding mode
- ▶ Regions  $R_2$  and  $R_3$  equipped with aux. dynamics  $y' = f_2(y) = f_{aux,A}(y)$  and  $y' = f_3(y) = f_{aux,B}(y)$ , resp., to mimic state jump
- ▶ Regions R<sub>1</sub> and R<sub>4</sub> equipped with DAE-forming dynamics y' = f<sub>1</sub>(y) = f<sub>df,A</sub>(y) and y' = f<sub>4</sub>(y) = f<sub>df,B</sub>(y), resp., to recover original dynamics in sliding mode
- ► E.g.,  $w' = 0 \implies \theta_1 f_{df,A}(y) + \theta_2 f_{aux,A}(y) = f_A(y)$ (sliding mode)
- Conclusion: we have a PSS and can treat it with FESD

### Time optimal control of a car with a turbo accelerator

Example from [Avraam, 2000] solved with NOSNOC



### Time optimal control of a car with a turbo accelerator

Example from [Avraam, 2000] solved with NOSNOC





 $y(\cdot$ 



$$\min_{\substack{y,u(\cdot),s(\cdot)}} t(\tau_{\rm f}) + L(\tau_{\rm f})$$
  
s.t. 
$$y(0) = (z_0, 0)$$
$$y'(\tau) \in s(\tau) F_{\rm TF}(y(\tau), u(\tau))$$
$$-\bar{u} \leq u(\tau) \leq \bar{u}$$
$$\bar{s}^{-1} \leq s(\tau) \leq \bar{s}$$
$$-\bar{v} \leq v(\tau) \leq \bar{v} \tau \in [0, \tau_{\rm f}]$$
$$(q(\tau_{\rm f}), v(\tau_{\rm f})) = (q_{\rm f}, v_{\rm f})$$

# Scenario 1: turbo and nominal cost the same

 $c_{\rm N} = c_{\rm T}$ 



Moritz Diehl

# Scenario 2: Turbo is Expensive

 $c_{\rm N} < c_{\rm T}$ 



Moritz Diehl

# NOSNOC vs MILP/MINLP formulations

Benchmark on time-optimal control problem of a car with turbo



- compare CPU time as function of number of control intervals N (left) and solution accuracy (right)
- $\blacktriangleright$  MILP (Gurobi): solve problem with fixed T until indefeasibly happens with grid search in T
- MILP/MINLP and NOSNOC-Std no switch detection = low accuracy



#### Conclusions

- Mathematical Programs with Complementarity Constraints (MPCC) are a powerful tool to formulate and solve nonsmooth and nonconvex optimization problems.
- Time-freezing allows us to transform systems with state jumps of level NSD3 to the easier level NSD2.
- Finite Elements with Switch Detection (FESD) allow highly accurate simulation and optimal control for switched systems of level NSD2.



#### Conclusions

- Mathematical Programs with Complementarity Constraints (MPCC) are a powerful tool to formulate and solve nonsmooth and nonconvex optimization problems.
- Time-freezing allows us to transform systems with state jumps of level NSD3 to the easier level NSD2.
- Finite Elements with Switch Detection (FESD) allow highly accurate simulation and optimal control for switched systems of level NSD2.

#### Outlook

- ▶ Time-freezing for multiple and simultaneous impacts with friction (work in progress)
- Time-freezing for more general hybrid automaton
- > Do generic time-freezing principles, easily applicable to *any* system with state jumps, exist?



- A time-freezing approach for numerical optimal control of nonsmooth differential equations with state jumps.
   A. Nurkanović, T. Sartor, S. Albrecht, and M. Diehl, IEEE Cont. Sys. Lett., 2021.
- Continuous optimization for control of hybrid systems with hysteresis via time-freezing A. Nurkanović and M. Diehl, IEEE Cont. Sys. Lett., 2022.
- The Time-Freezing Reformulation for Numerical Optimal Control of Complementarity Lagrangian Systems with State Jumps.
   A. Nurkanović, S. Albrecht, B. Brogliato, and M. Diehl, arXiv preprint 2022
- Set-Valued Rigid Body Dynamics for Simultaneous Frictional Impact. Mathew Halm and Michael Posa, arXiv Preprint, 2021.

Thank you very much for your attention!