

# Grid Integration of Airborne Wind Energy

## AWESCO Kick-off meeting

Elena Malz

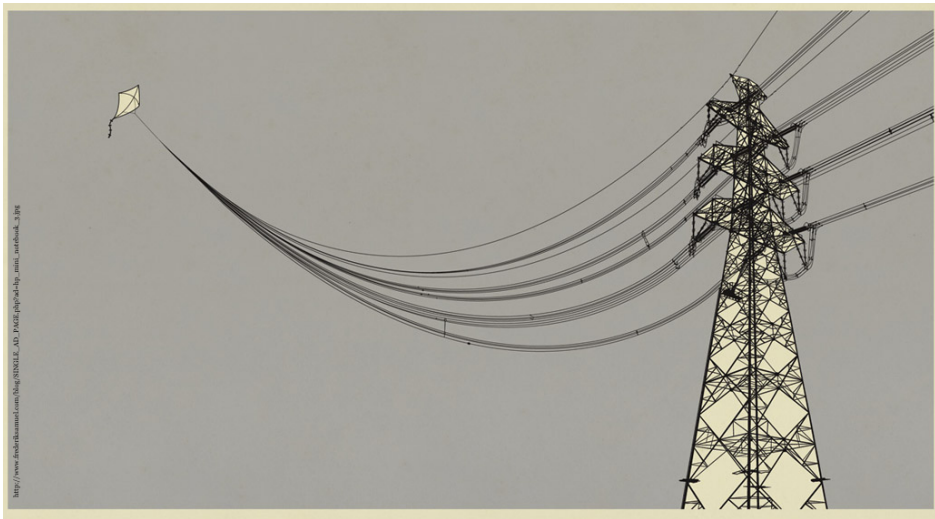
Department of Signals & Systems  
Chalmers University of Technology, Gothenburg, Sweden

March 2, 2016



Background: Wind Power Systems, Aalborg University  
Research Topic: Optimization of the Electro-Mechanical & Grid Interactions for AWE systems  
Location: University of Chalmers, Göteborg, Sweden  
Supervisor: Sébastien Gros

- 1 Background & Motivation
- 2 Project Description and Project Plan
- 3 Results



[http://www.federthamoud.com/blog/SINGLE\\_AD\\_PAGE.php?ad=hp\\_minimal\\_norbook\\_3\\_BW](http://www.federthamoud.com/blog/SINGLE_AD_PAGE.php?ad=hp_minimal_norbook_3_BW)

**What is the problem of integrating renewables into the power grid?**

## What is the problem of integrating renewables into the power grid?

### Grid codes ?

All power generators have to comply with certain requirements to ensure grid safety

## What is the problem of integrating renewables into the power grid?

- Active power control (Storage?)

### Grid codes ?

All power generators have to comply with certain requirements to ensure grid safety

## What is the problem of integrating renewables into the power grid?

- Active power control (Storage?)
- Modulation of active and reactive power

### Grid codes ?

All power generators have to comply with certain requirements to ensure grid safety



## What is the problem of integrating renewables into the power grid?

- Active power control (Storage?)
- Modulation of active and reactive power
- Limitation on harmonics

### Grid codes ?

All power generators have to comply with certain requirements to ensure grid safety

## What is the problem of integrating renewables into the power grid?

- Active power control (Storage?)
- Modulation of active and reactive power
- Limitation on harmonics
- ...

### Grid codes ?

All power generators have to comply with certain requirements to ensure grid safety

## What is the problem of integrating renewables into the power grid?

- Active power control (Storage?)
- Modulation of active and reactive power
- Limitation on harmonics
- ...

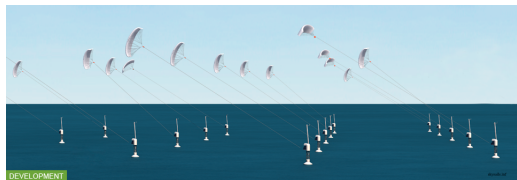
### Grid codes ?

All power generators have to comply with certain requirements to ensure grid safety

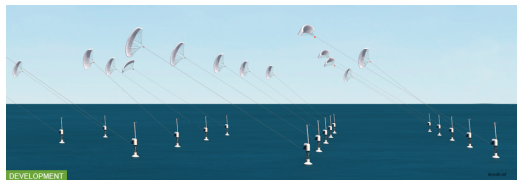
This problems probably also appear for AWES.  
But in which extend? What are the differences? And how can we deal with that?

- 1 Background & Motivation
- 2 Project Description and Project Plan
- 3 Results

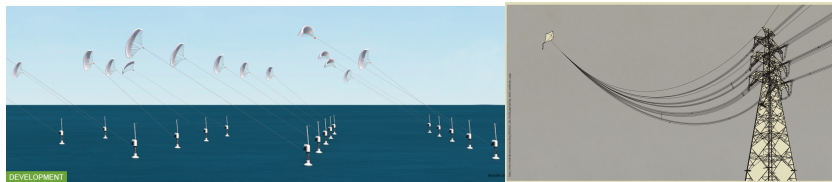
# Project keypoints



- 1 Study/Optimize the power output of an AWE farm

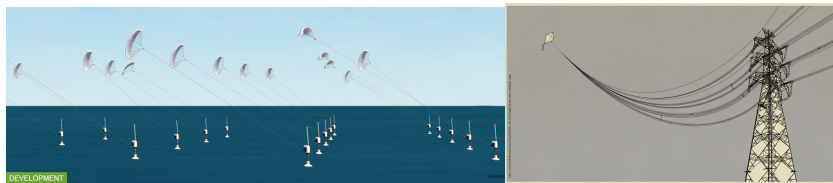


- 1 Study/Optimize the power output of an AWE farm
- 2 Generator & power electronic constraints (Electro-Mechanical Interactions)



- 1 Study/Optimize the power output of an AWE farm
- 2 Generator & power electronic constraints (Electro-Mechanical Interactions)
- 3 Interaction between a strong/weak power grid and an AWE farm? (Grid Interactions)





- 1 Study/Optimize the power output of an AWE farm
- 2 Generator & power electronic constraints (Electro-Mechanical Interactions)
- 3 Interaction between a strong/weak power grid and an AWE farm? (Grid Interactions)
- 4 How to implement grid-code compliance in practice?

## First Year

Model of large scale electro-mechanical power systems and their interaction with the power grid.

Study control and optimization theory.

## Second Year

4 month secondment in Freiburg: Numerical and large scale optimization. Solutions for AWE systems with grid interactions.

## Third Year

Methods applications to a test scenario defined by Skysails.

2 month secondment at Skysails.

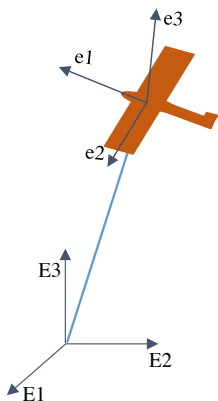
- 1 Background & Motivation
- 2 Project Description and Project Plan
- 3 Results

# Development of a kite model (Python/Casadi)

# Development of a kite model (Python/Casadi)

S. Gros, M. Zanon and M. Diehl, "A relaxation strategy for the optimization of Airborne Wind Energy systems,"

Horn, S., Gros, S. och Diehl, M. (2013) Numerical Trajectory Optimization for Airborne Wind Energy Systems



... flying a circular trajectory

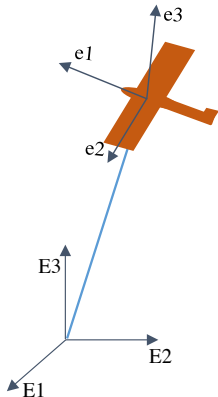
# Development of a kite model (Python/Casadi)

S. Gros, M. Zanon and M. Diehl, "A relaxation strategy for the optimization of Airborne Wind Energy systems,"

Horn, S., Gros, S. och Diehl, M. (2013) Numerical Trajectory Optimization for Airborne Wind Energy Systems

## Goal

- 1 Optimize power output



... flying a circular trajectory

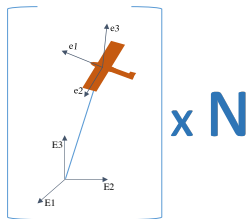
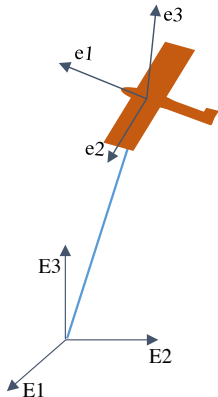
# Development of a kite model (Python/Casadi)

S. Gros, M. Zanon and M. Diehl, "A relaxation strategy for the optimization of Airborne Wind Energy systems,"

Horn, S., Gros, S. och Diehl, M. (2013) Numerical Trajectory Optimization for Airborne Wind Energy Systems

## Goal

- 1 Optimize power output
- 2 Scale up system to AWE farm



... flying a circular trajectory

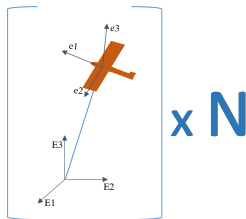
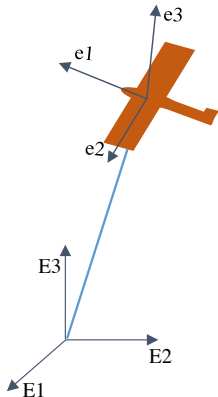
# Development of a kite model (Python/Casadi)

S. Gros, M. Zanon and M. Diehl, "A relaxation strategy for the optimization of Airborne Wind Energy systems,"

Horn, S., Gros, S. och Diehl, M. (2013) Numerical Trajectory Optimization for Airborne Wind Energy Systems

## Goal

- 1 Optimize power output
- 2 Scale up system to AWE farm



... flying a circular trajectory

**So, how is this optimization problem implemented?**

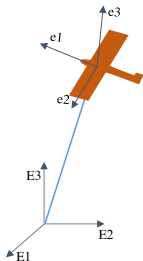


## Dynamics:

$$\begin{bmatrix} m \cdot \mathbf{I} & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $E$   
given by:

$$\mathbf{w} \in \mathbb{R}^3$$

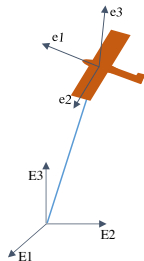
## Dynamics:

$$\begin{bmatrix} m \cdot \mathbf{I} & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-z\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $E$   
given by:

$$\mathbf{w} \in \mathbb{R}^3$$

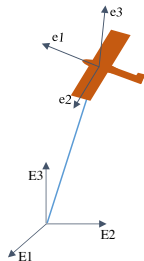
## Dynamics:

$$\begin{bmatrix} m \cdot \mathbf{I} & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-z\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$
- Apparent wind in the fixed frame:  $\mathbf{v} = \dot{\mathbf{p}} - \mathbf{w}$
- Apparent wind in the kite frame:  $\mathbf{v}_e = R^\top (\dot{\mathbf{p}} - \mathbf{w})$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $E$   
given by:

$$\mathbf{w} \in \mathbb{R}^3$$

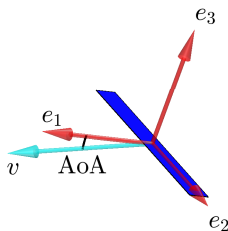
## Dynamics:

$$\begin{bmatrix} m \cdot \mathbf{I} & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-\mathbf{z}\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$
- Apparent wind in the fixed frame:  $\mathbf{v} = \dot{\mathbf{p}} - \mathbf{w}$
- Apparent wind in the kite frame:  $\mathbf{v}_e = R^\top (\dot{\mathbf{p}} - \mathbf{w})$
- Angle of Attack:  $\tan(\text{AoA}) = -\frac{\mathbf{e}_3^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $\mathbf{w}$   
given by:

$$\mathbf{w} \in \mathbb{R}^3$$

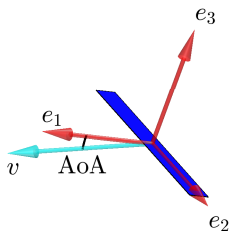
## Dynamics:

$$\begin{bmatrix} m \cdot I & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} -\mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-\mathbf{z}\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$
- Apparent wind in the fixed frame:  $\mathbf{v} = \dot{\mathbf{p}} - \mathbf{w}$
- Apparent wind in the kite frame:  $\mathbf{v}_e = R^\top (\dot{\mathbf{p}} - \mathbf{w})$
- Angle of Attack:  $\tan(\text{AoA}) = -\frac{\mathbf{e}_3^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Side-slip:  $\tan(\text{Slip}) = \frac{\mathbf{e}_2^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $\mathbf{E}$   
given by:

$$\mathbf{w} \in \mathbb{R}^3$$

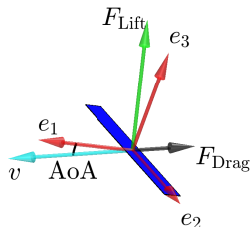
## Dynamics:

$$\begin{bmatrix} m \cdot I & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-z\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$
- Apparent wind in the fixed frame:  $\mathbf{v} = \dot{\mathbf{p}} - \mathbf{w}$
- Apparent wind in the kite frame:  $\mathbf{v}_e = R^\top (\dot{\mathbf{p}} - \mathbf{w})$
- Angle of Attack:  $\tan(\text{AoA}) = -\frac{\mathbf{e}_3^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Side-slip:  $\tan(\text{Slip}) = \frac{\mathbf{e}_2^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Drag force:  $\mathbf{F}_{\text{Drag}} = -\frac{1}{2}\rho AC_D(\text{AoA}) \|\mathbf{v}\| \mathbf{v}$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $\mathbf{E}$  given by:

$$\mathbf{w} \in \mathbb{R}^3$$

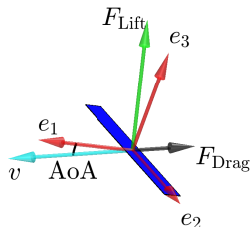
## Dynamics:

$$\begin{bmatrix} m \cdot I & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-z\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$
- Apparent wind in the fixed frame:  $\mathbf{v} = \dot{\mathbf{p}} - \mathbf{w}$
- Apparent wind in the kite frame:  $\mathbf{v}_e = R^\top (\dot{\mathbf{p}} - \mathbf{w})$
- Angle of Attack:  $\tan(\text{AoA}) = -\frac{\mathbf{e}_3^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Side-slip:  $\tan(\text{Slip}) = \frac{\mathbf{e}_2^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Drag force:  $\mathbf{F}_{\text{Drag}} = -\frac{1}{2}\rho AC_D(\text{AoA}) \|\mathbf{v}\| \mathbf{v}$
- Lift force:  $\mathbf{F}_{\text{Lift}} = \frac{1}{2}\rho AC_L(\text{AoA}) \|\mathbf{v}\| \mathbf{v} \wedge \mathbf{e}_2$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $\mathbf{E}$  given by:

$$\mathbf{w} \in \mathbb{R}^3$$

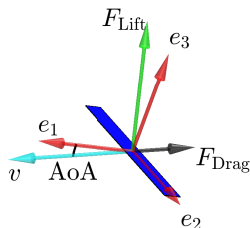
## Dynamics:

$$\begin{bmatrix} m \cdot I & \mathbf{p} \\ \mathbf{p}^\top & 0 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{p}} \\ z \end{bmatrix} = \begin{bmatrix} \mathbf{F}_g \\ -\dot{\mathbf{p}}^\top \dot{\mathbf{p}} - L\ddot{L} - \dot{L}^2 \end{bmatrix}$$

$$\dot{R} = R\omega_\times$$

$$J\dot{\omega} = \mathbf{T} - \omega \times J\omega$$

- Tether force:  $-z\mathbf{p}$ , magnitude is  $F_{\text{Tether}} = zL$
- Apparent wind in the fixed frame:  $\mathbf{v} = \dot{\mathbf{p}} - \mathbf{w}$
- Apparent wind in the kite frame:  $\mathbf{v}_e = R^\top (\dot{\mathbf{p}} - \mathbf{w})$
- Angle of Attack:  $\tan(\text{AoA}) = -\frac{\mathbf{e}_3^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Side-slip:  $\tan(\text{Slip}) = \frac{\mathbf{e}_2^\top (\dot{\mathbf{p}} - \mathbf{w})}{\mathbf{e}_1^\top (\dot{\mathbf{p}} - \mathbf{w})}$
- Drag force:  $\mathbf{F}_{\text{Drag}} = -\frac{1}{2}\rho AC_D(\text{AoA}) \|\mathbf{v}\| \mathbf{v}$
- Lift force:  $\mathbf{F}_{\text{Lift}} = \frac{1}{2}\rho AC_L(\text{AoA}) \|\mathbf{v}\| \mathbf{v} \wedge \mathbf{e}_2$
- Power in drag-mode:  $P = F_{\text{Power}} \mathbf{e}_1^\top \dot{\mathbf{p}}$



Rotation:

$$R = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \mathbf{e}_3 \end{bmatrix}$$

Wind in the fixed frame  $\mathbf{E}$  given by:

$$\mathbf{w} \in \mathbb{R}^3$$



# Power optimization problem

$$\max_{\mathbf{x}, z, R, \mathbf{u}, t_\pi} \quad \frac{1}{t_\pi} \int_0^{t_\pi} P(\mathbf{x}, z, \mathbf{u}) dt$$

*Cost Function*

$$\text{s.t.} \quad \mathbf{F}(\dot{\mathbf{x}}, \mathbf{x}, R, z, \mathbf{u}, \mathbf{w}) = 0$$

*Dynamics*

$$\boldsymbol{\pi} = 0, \quad \mathbf{c} = 0$$

*Periodic & tether constraints*

$$\mathbf{h}(\mathbf{x}, z, \mathbf{u}, \mathbf{w}) \leq 0$$

*Path constraints*

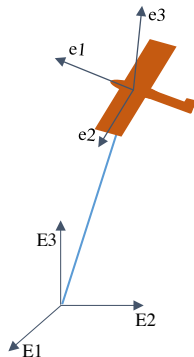
# Power optimization problem

$$\begin{aligned} \max_{\mathbf{x}, z, R, \mathbf{u}, t_\pi} \quad & \frac{1}{t_\pi} \int_0^{t_\pi} P(\mathbf{x}, z, \mathbf{u}) dt \\ \text{s.t.} \quad & \mathbf{F}(\dot{\mathbf{x}}, \mathbf{x}, R, z, \mathbf{u}, \mathbf{w}) = 0 \\ & \boldsymbol{\pi} = 0, \quad \mathbf{c} = 0 \\ & \mathbf{h}(\mathbf{x}, z, \mathbf{u}, \mathbf{w}) \leq 0 \end{aligned}$$

**Differential states:**  $\mathbf{x} = \{\mathbf{p}, \dot{\mathbf{p}}, \boldsymbol{\omega}\}, R, E$

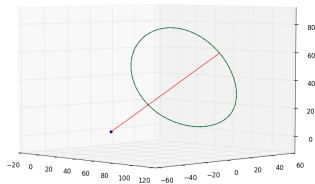
**Algebraic state:**  $z \in \mathbb{R}$

**Inputs:**  $\mathbf{u}$  for control surfaces



# Things to be careful about..

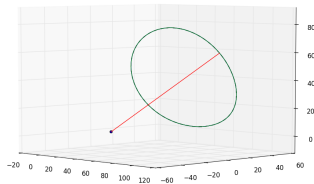
- Good initial guess needed



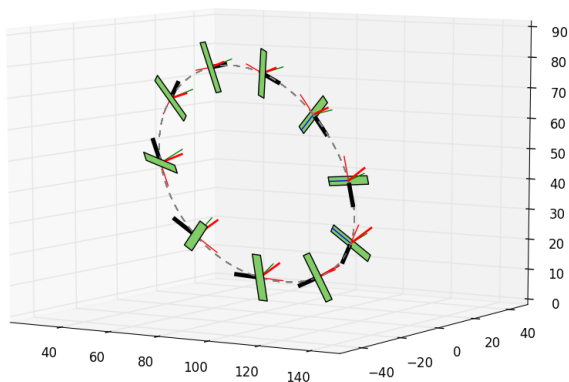
# Things to be careful about..

- Good initial guess needed
- Aerodynamic forces and moments create nonlinear feedback loops  
 $T_A(x, R, w, u)$  and  $F_A(x, R, w, u)$

Use of **homotopy**, i.e. switch from artificial forces to the 'real' physical model



Just a beginning...



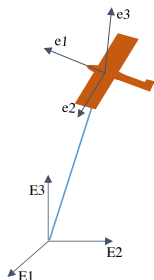
**Optimal trajectory for one cycle when optimizing for maximum power output**

## What's next?

- Add wind shear
- Power optimization for pumping mode
- Introduce cable drag
- Scale up to AWE farm

## What has been done so far:

- Studies on Optimization & Optimal Control
- First steps in development of an AWE model with the aim of optimizing power output



## Future Research

- Include electrical drive constraints
- Study harmonics in power output