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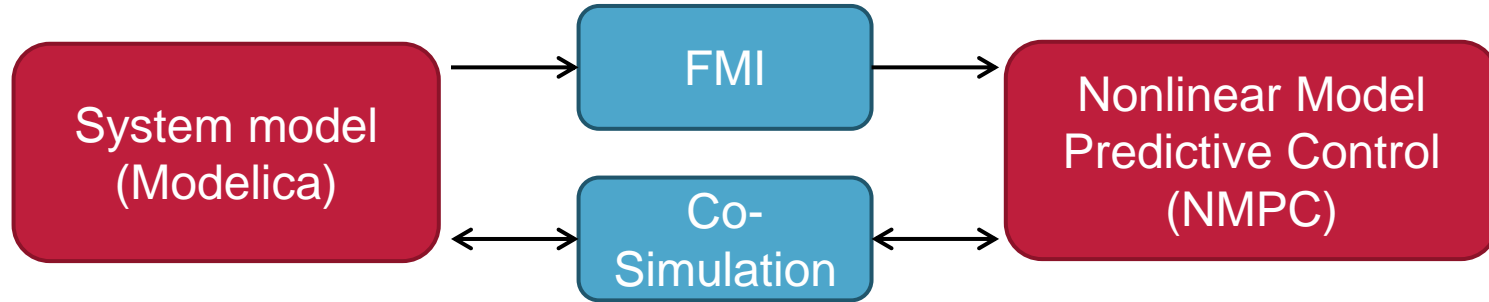
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# A Short Framework for Prototyping Nonlinear Model Predictive Control Loops

M. Nöding, M. Gräber, C. Kirches, W. Tegethoff

# Introduction and Motivation



- Convenient tools for modeling and simulation
- Many different model libraries
- Mainly used for simulation
- Use system knowledge to improve control performance
- Highly efficient algorithms exist
- Designing and tuning is a complex task
- Very important: good system models

# Contents

- Optimal Control Task and NMPC
- Used Software
- Simulation of Vapour Compression Cycle
- Simulation of Thermoactive Ceiling
- Conclusion

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# Optimal Control Task and NMPC

Cost function

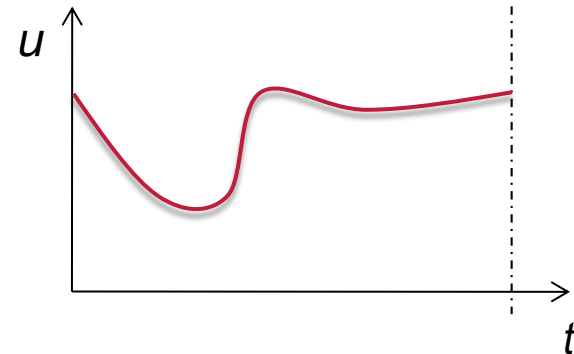
$$C = a \int_0^{\tau} (T - T_{\text{set}})^2 dt + b \int_0^{\tau} P dt$$

Dynamic system model  
(ODE)

$$\dot{x}(t) = f(x(t), u(t))$$

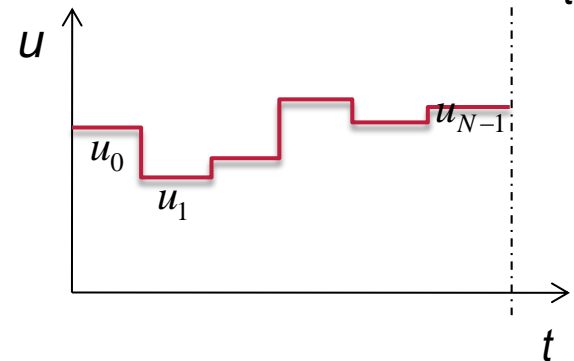
Optimal Control Problem  
(OCP)

$$\begin{aligned} & \min_{x(\cdot), u(\cdot)} C(x(\cdot), u(\cdot)) \\ \text{s.t. } & \dot{x}(t) = f(x(t), u(t)) \\ & 0 \leq c(x(t), u(t)) \\ & x(0) = x_0 \end{aligned}$$



Infinite dimensional problem  
(NLP)

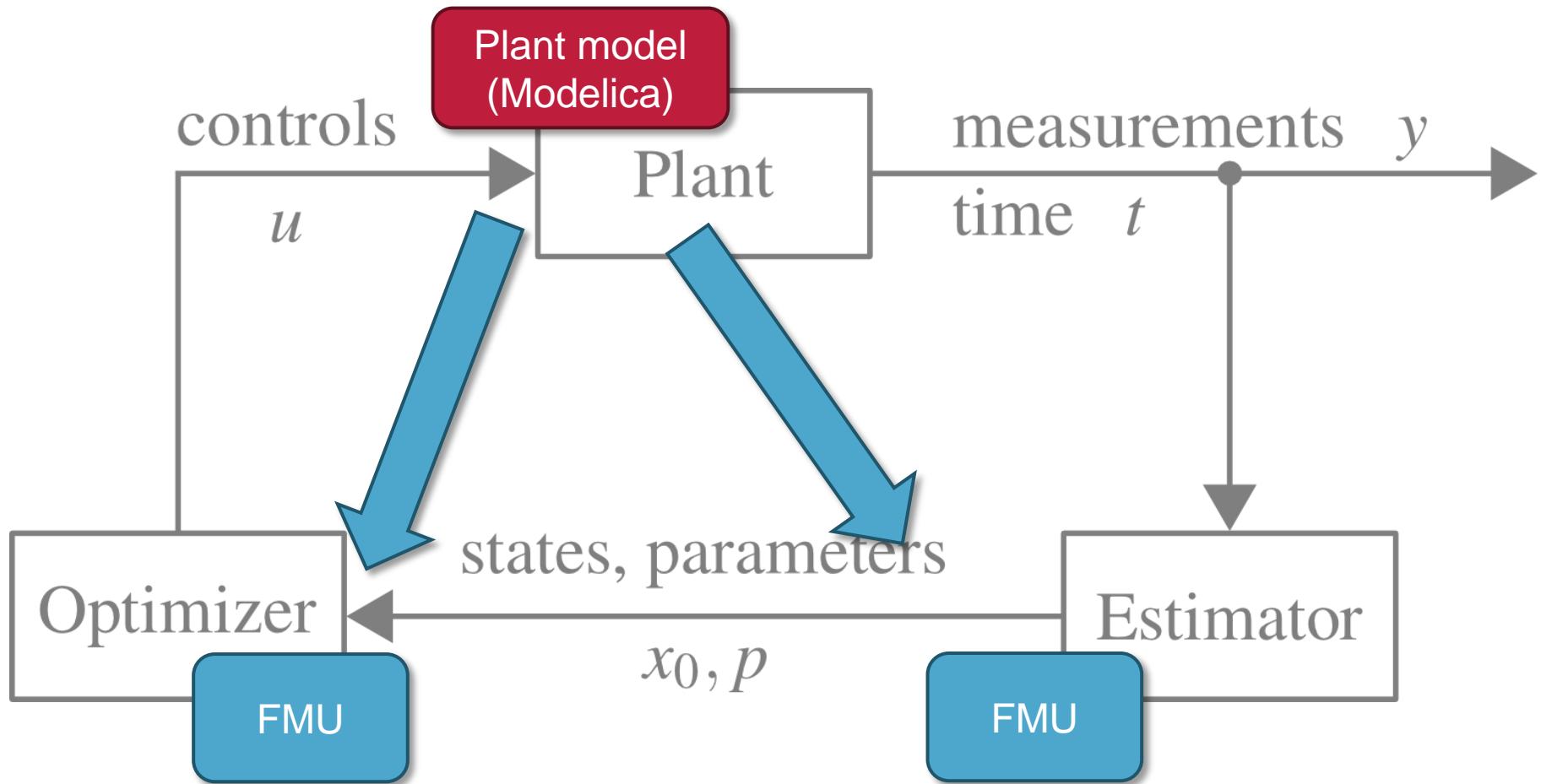
$$\begin{aligned} & \min_{s_0, \dots, s_N, u_0, \dots, u_{N-1}} \sum_{i=0}^N l_i(s_i, u_i) \\ \text{s.t. } & s_{i+1} = x_i(\tau_{i+1}; s_i, u_i) \\ & 0 \leq c(s_i, u_i) \\ & s_0 = x_0 \end{aligned}$$



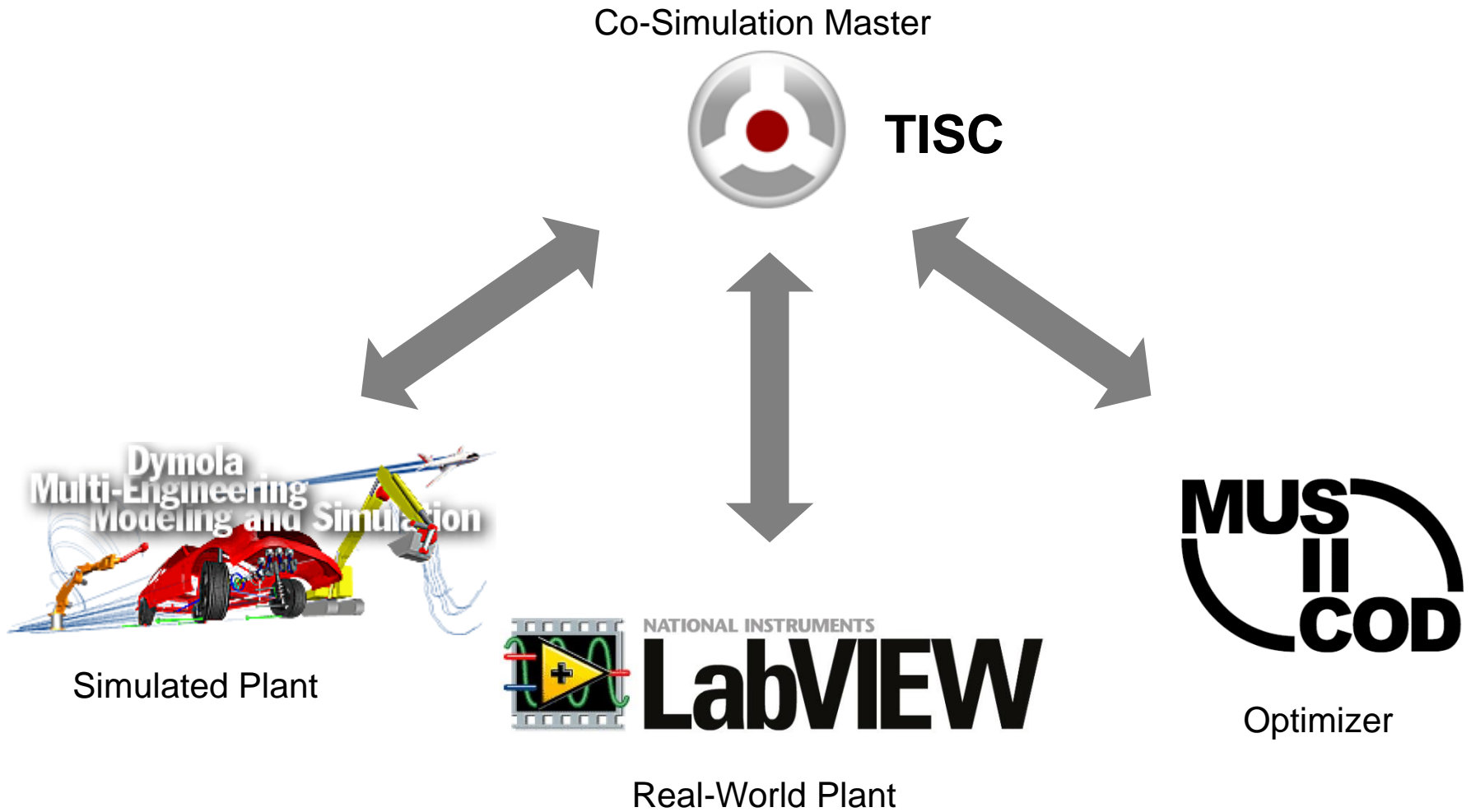
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# Used Software



# Used Software

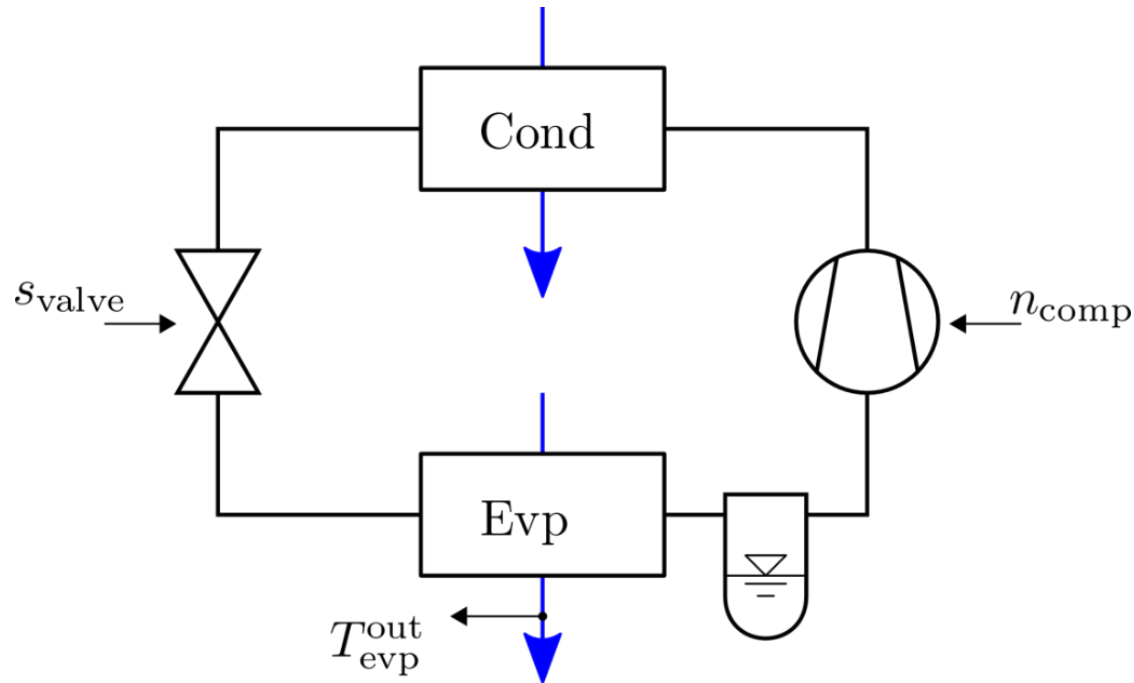




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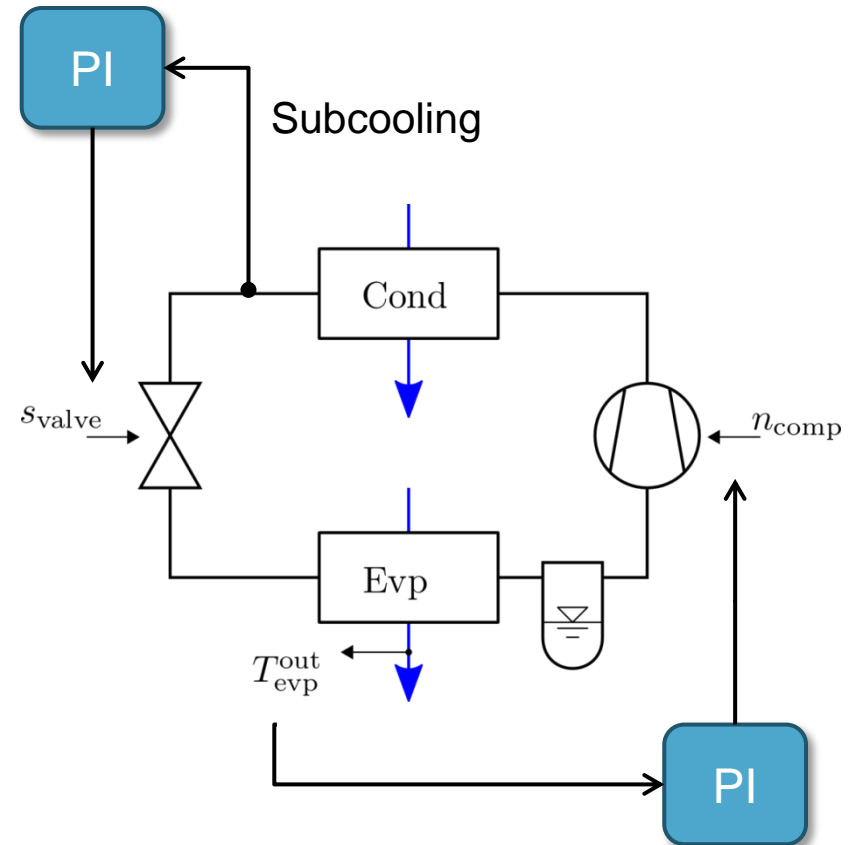
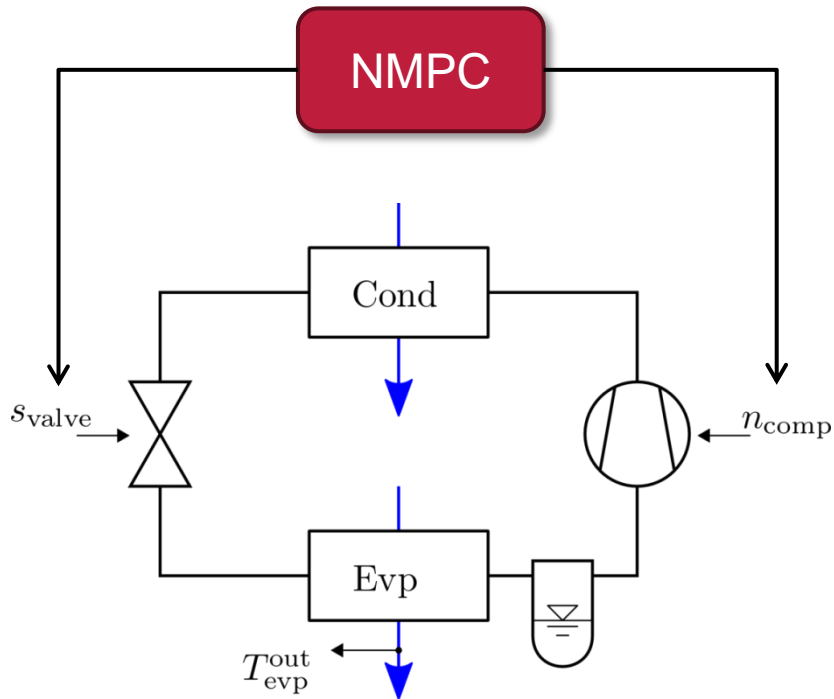
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# Simulation of Vapour Compression Cycle



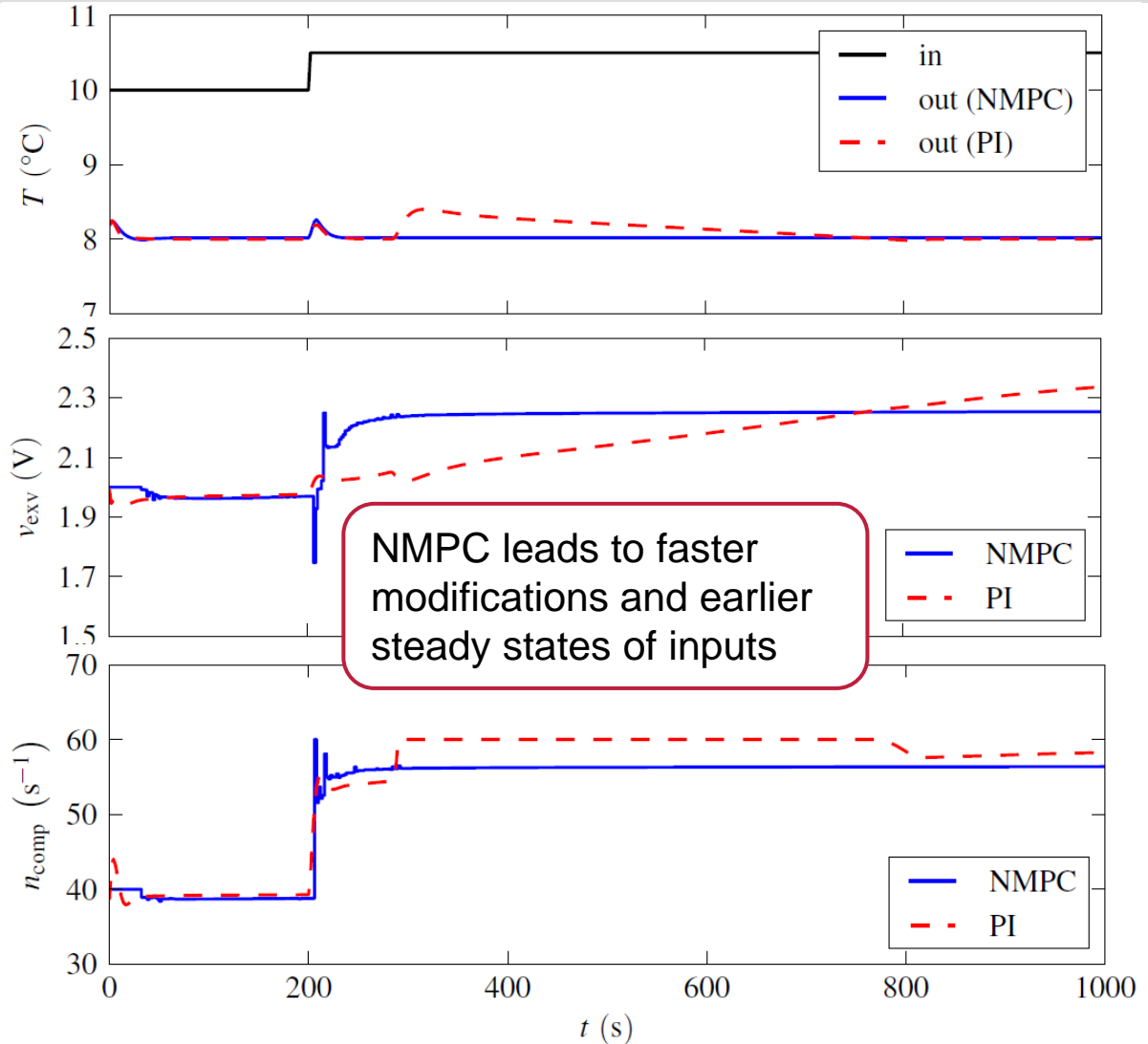
- Control inputs: expansion valve opening, compressor speed
- Goal 1: constant outlet temperature
- Goal 2: as less electrical energy as possible

# Simulation Experiment – Vapour Compression Cycle



# Simulation Results - Compression Cycle

*Inlet and outlet*  
Chilled water temperatures

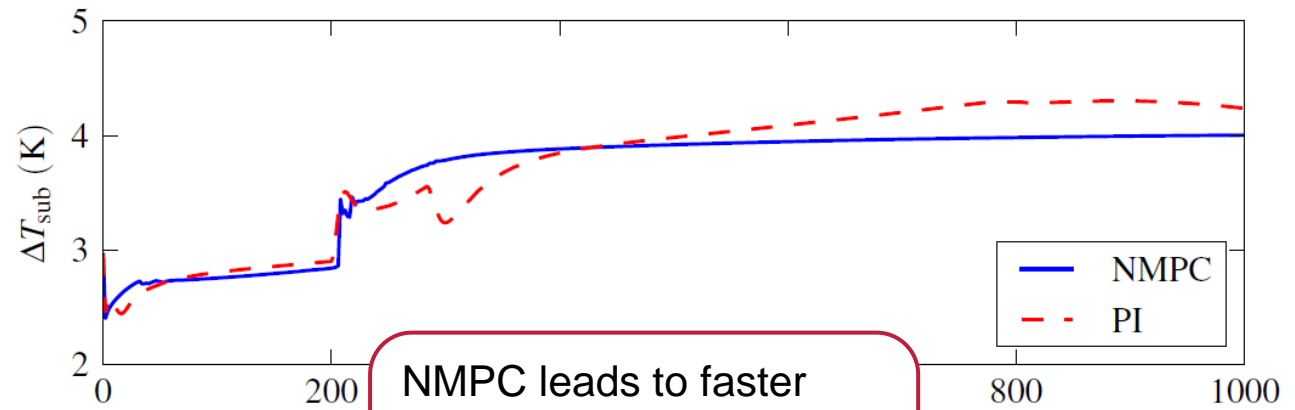


*Control input*  
Expansion valve opening

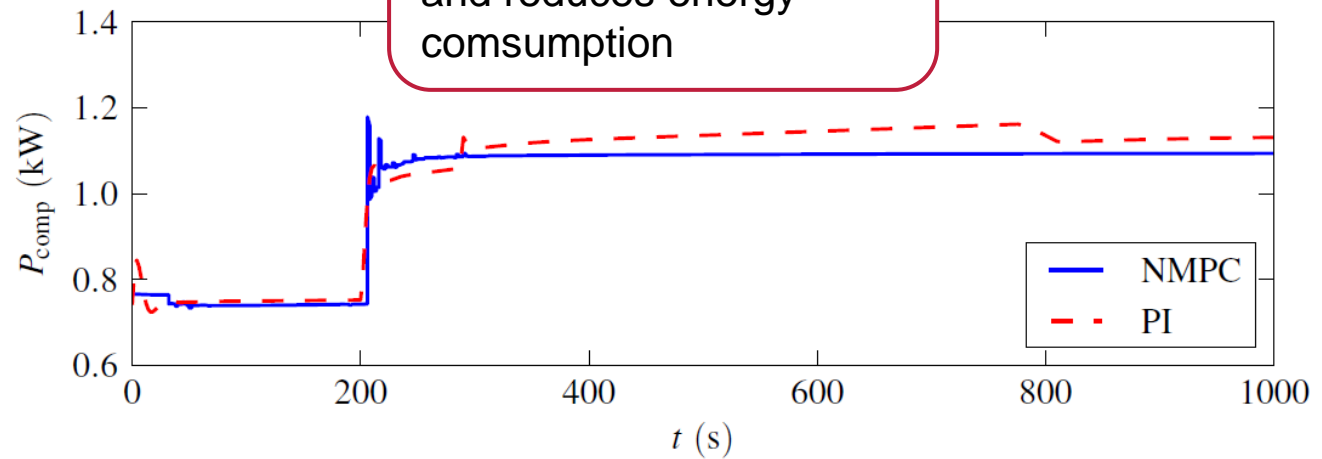
*Control input*  
Compressor speed

# Simulation Results – Vapour Compression Cycle

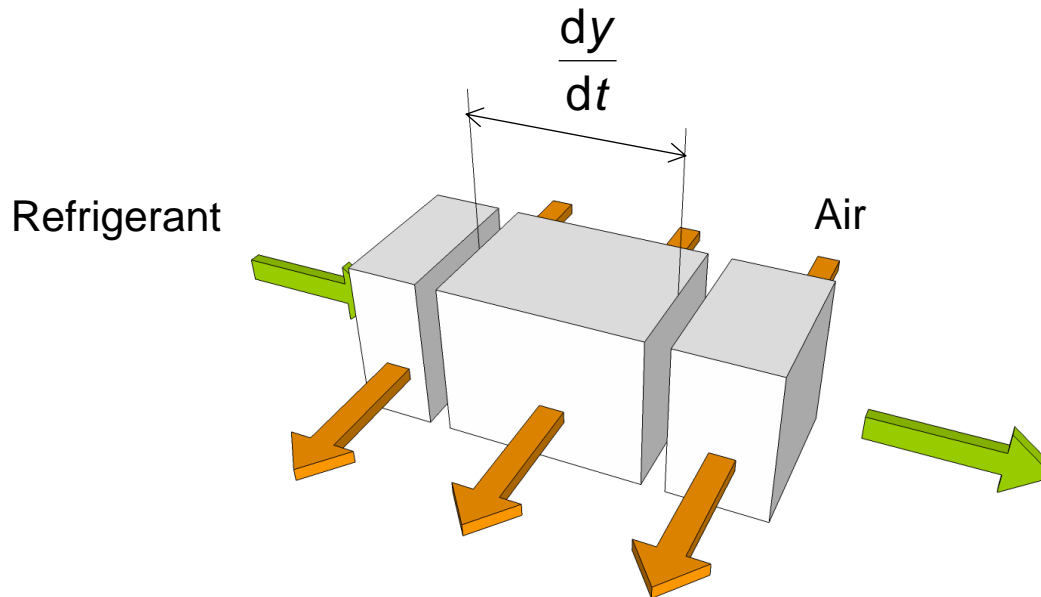
*Output*  
Refrigerant subcooling



*Output*  
Compressor power



# Steps to Speed Up Optimization - Heat Exchanger Model



- Dynamic control volumes
- Boundaries always at 1-phase / 2-phase transition point
- Mass and energy balance equations for each volume

# Steps to Speed Up Optimization - Real-Time Iteration

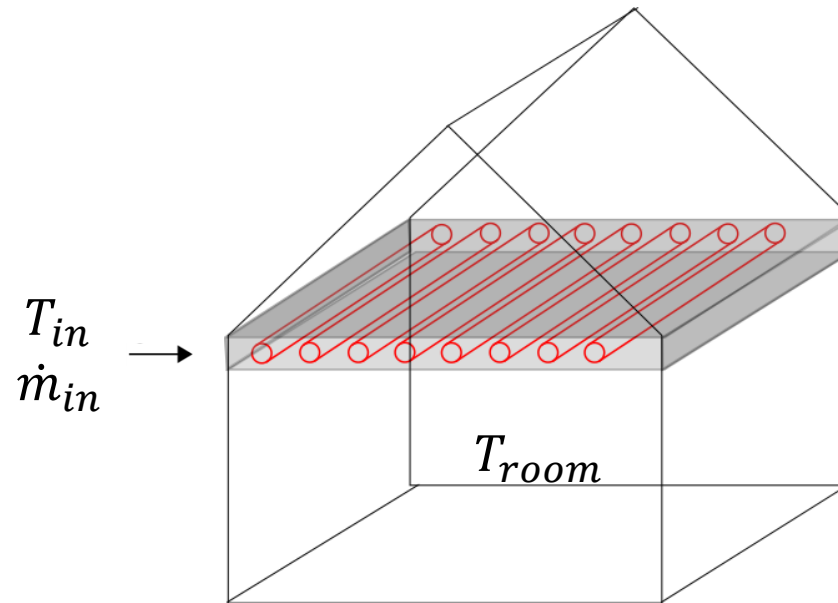
- Only one Sequential Quadratic Programming (SQP) iteration per NMPC sample

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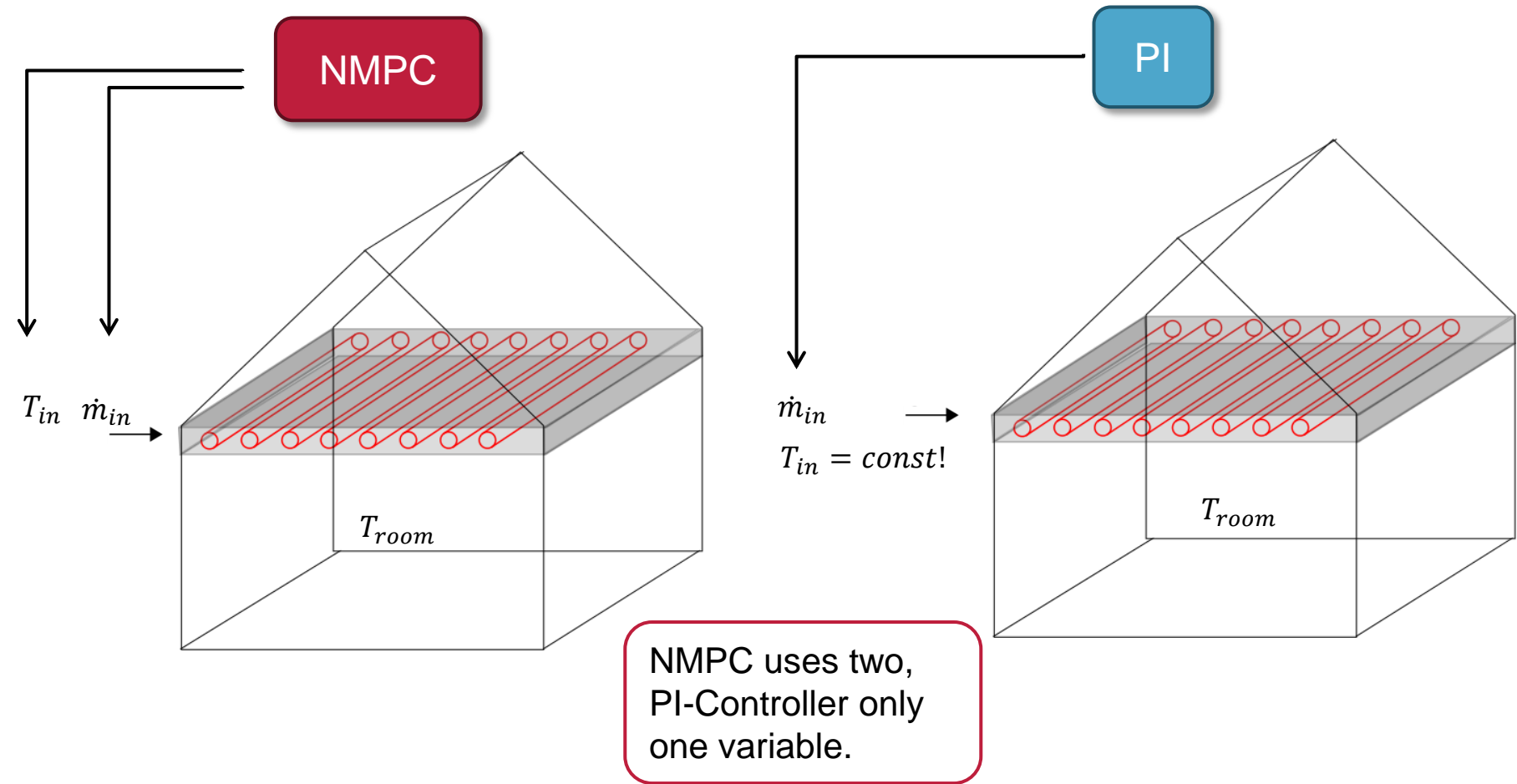


# Simulation of Thermoactive Ceiling



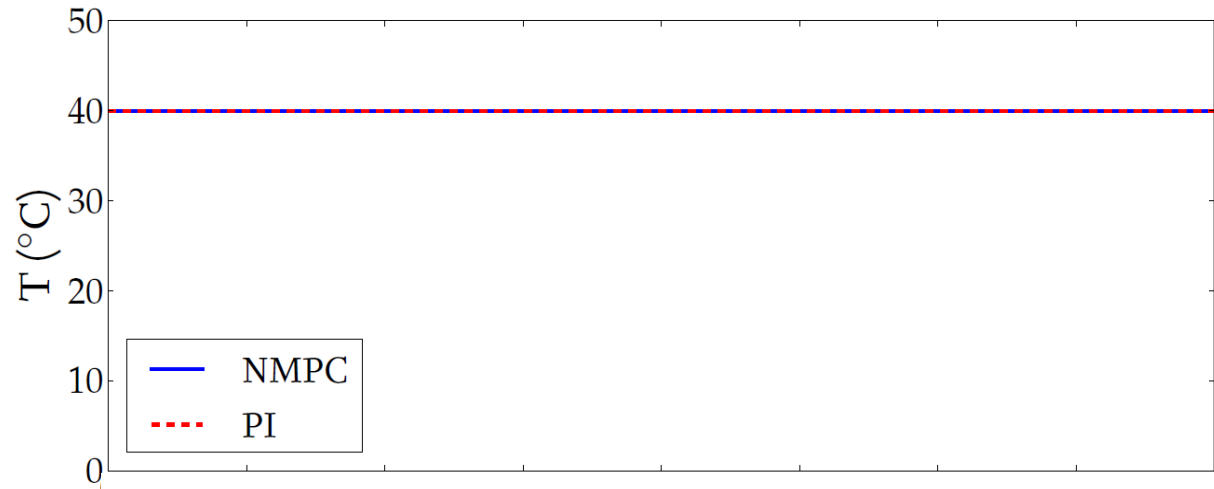
- Control inputs: inlet temperature, inlet massflow
- Goal 1: constant room temperature
- Goal 2: as less heating energy as possible

# Simulation Experiment - Thermoactive Ceiling

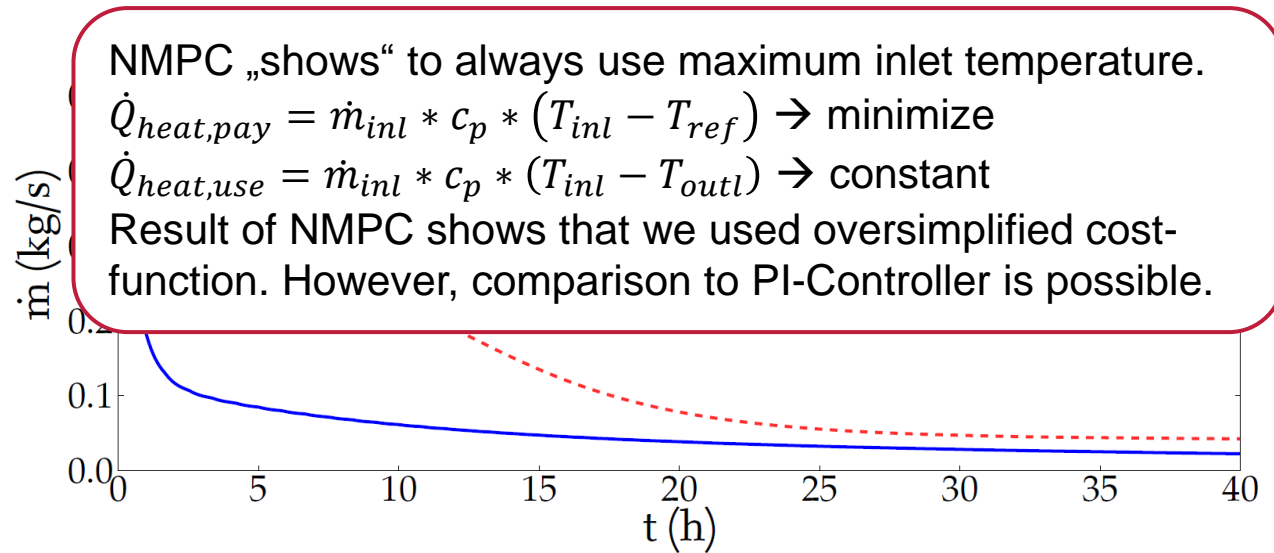


# Simulation Results – Thermoactive Ceiling

*Control input*  
Inlet temperature



*Control input*  
Inlet massflow



NMPC „shows“ to always use maximum inlet temperature.

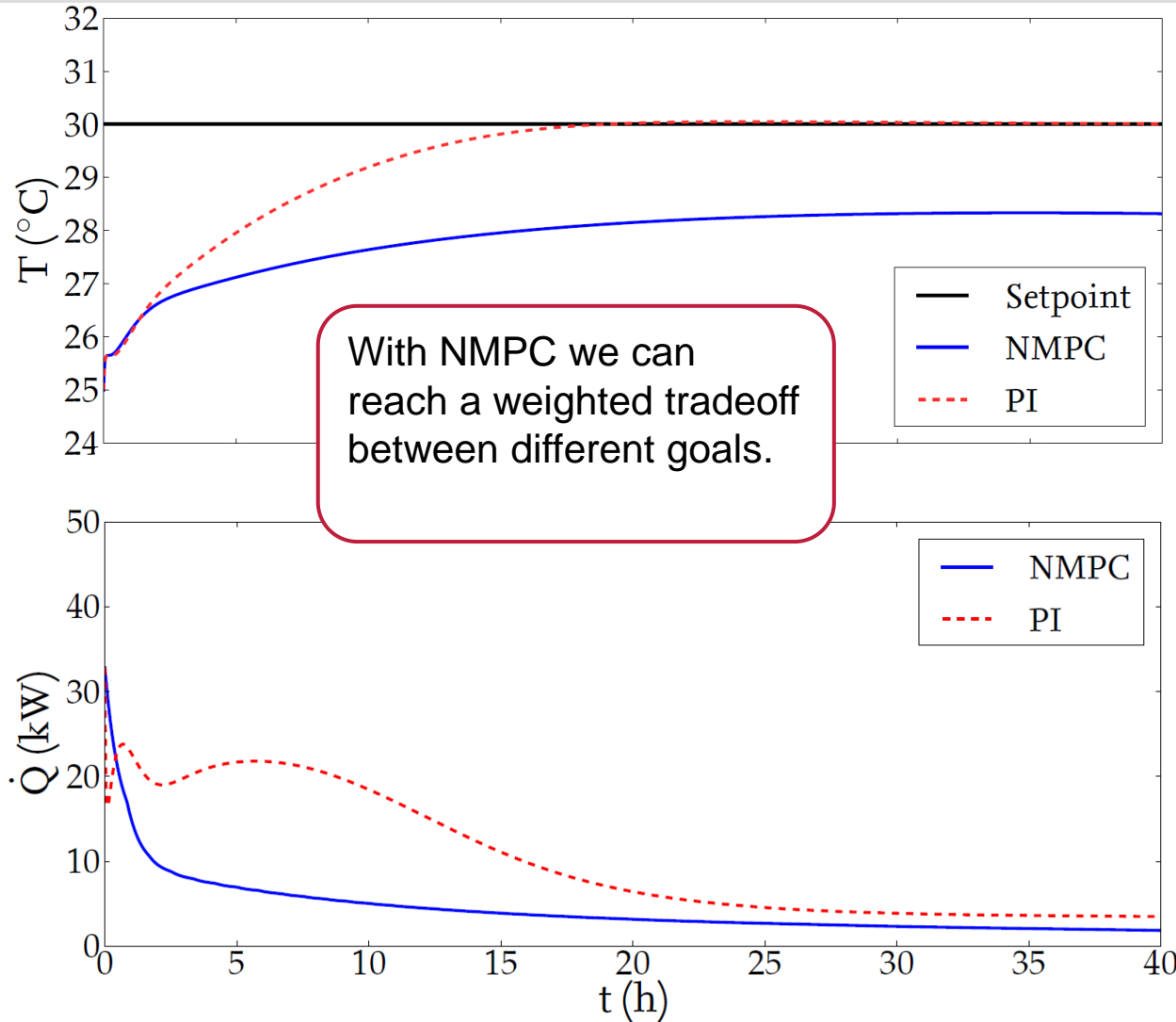
$$\dot{Q}_{heat,pay} = \dot{m}_{inl} * c_p * (T_{inl} - T_{ref}) \rightarrow \text{minimize}$$

$$\dot{Q}_{heat,use} = \dot{m}_{inl} * c_p * (T_{inl} - T_{outl}) \rightarrow \text{constant}$$

Result of NMPC shows that we used oversimplified cost-function. However, comparison to PI-Controller is possible.

# Simulation Results - Thermoactive Ceiling

*Output*  
Room Temperature



*Output*  
Heating energy

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# Conclusion

## Summary

- FMI successfully used in NMPC applications
- Control method for vapor compression presented
- Simulation and measurement results (not presented) show feasibility
- (Oversimplified) control method for climate control of buildings presented

## Future work

- Include Jacobian information (FMI 2.0)
- Extend model interface to hybrid DAE

# Additional Slides



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24. März 2015 | Michael Nöding | Using FMU for NMPC | Slide 23



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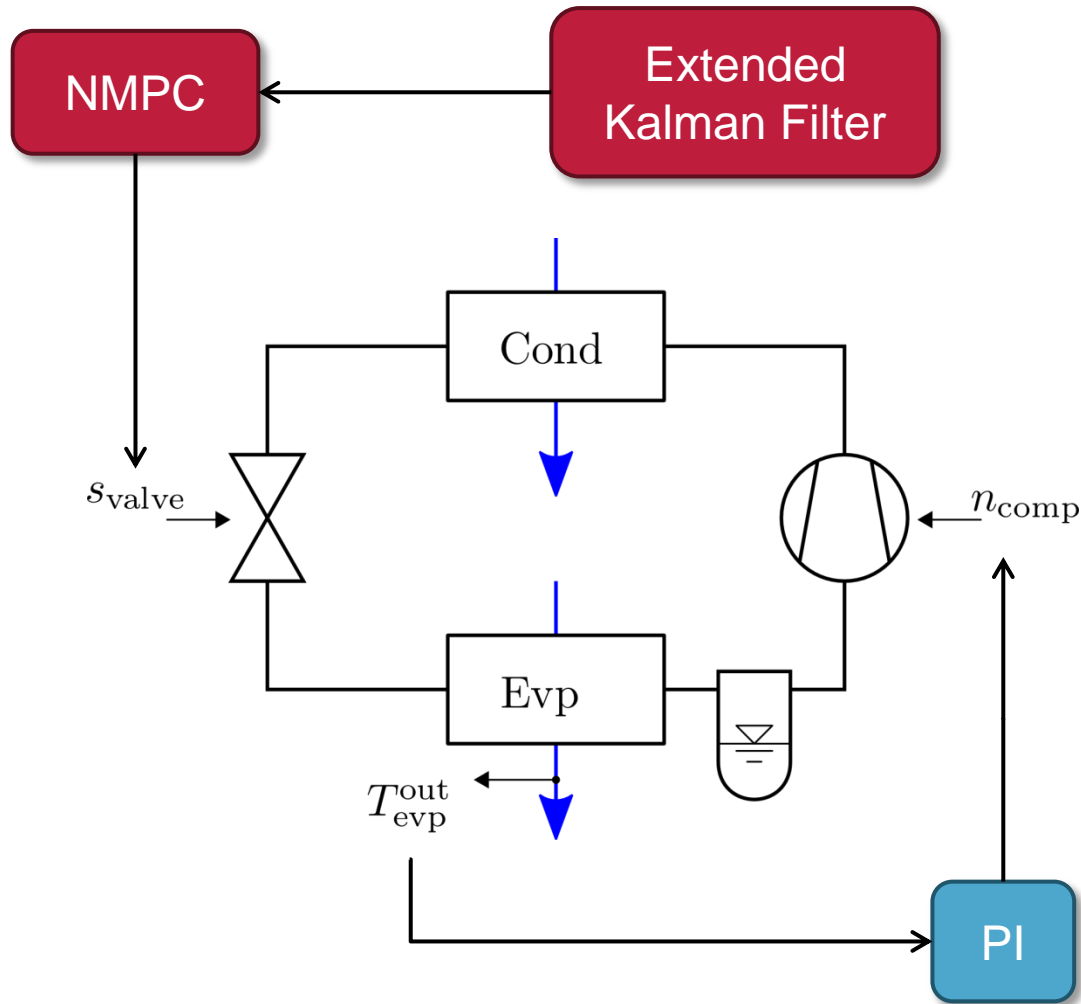


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# Real-World Application

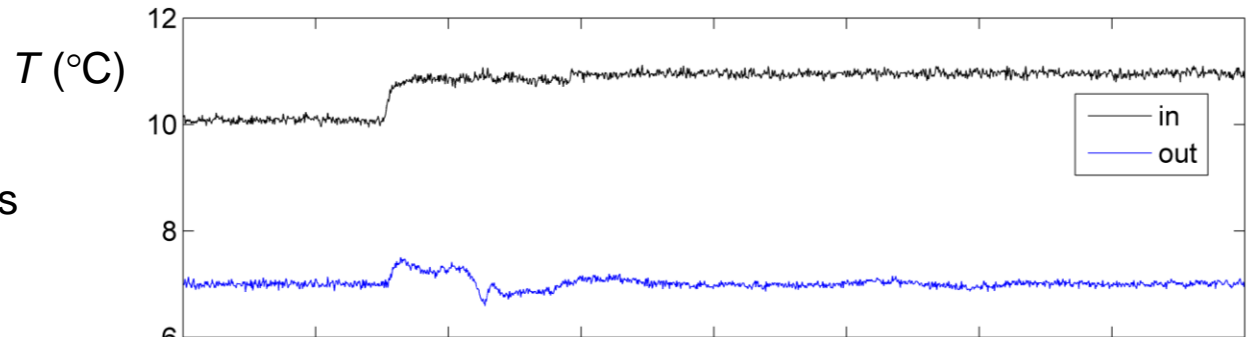




# Measurement Results

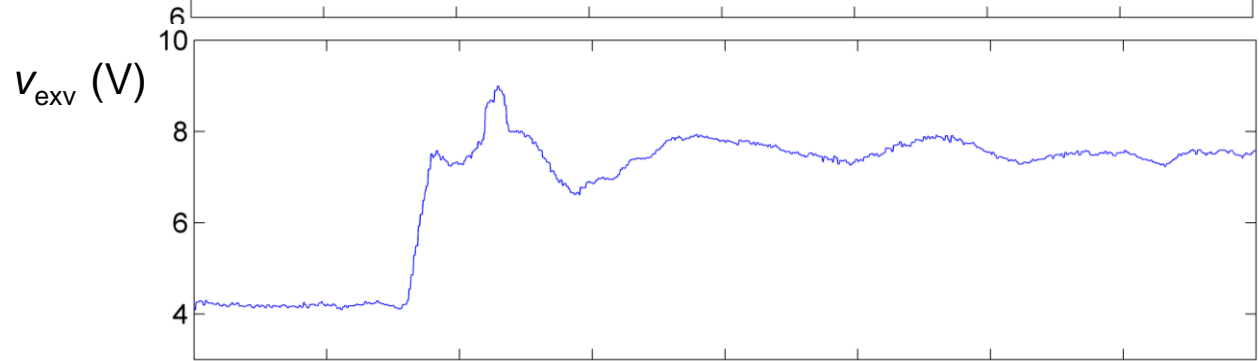
*Inlet and outlet*

Chilled water temperatures



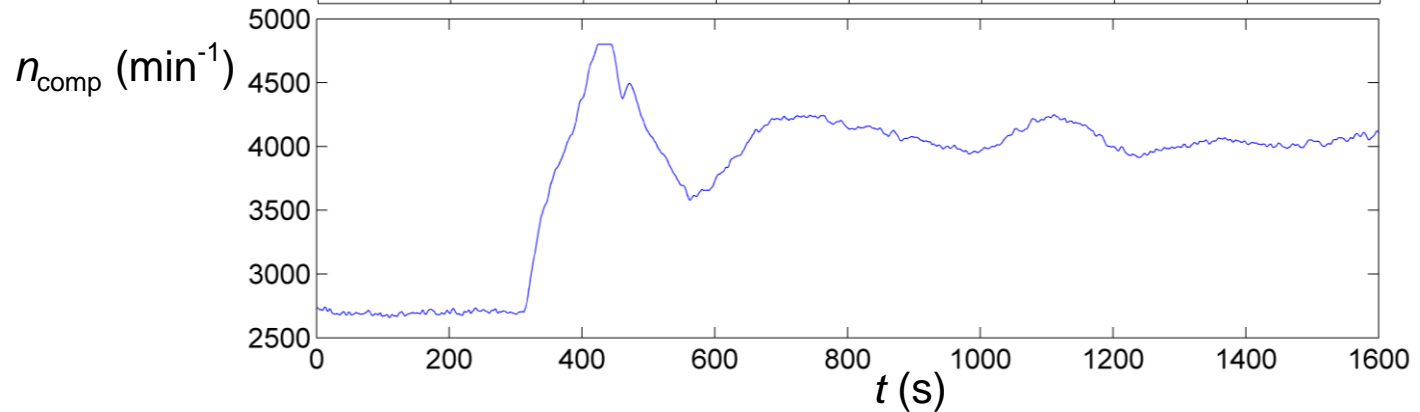
*Control input*

Expansion valve opening



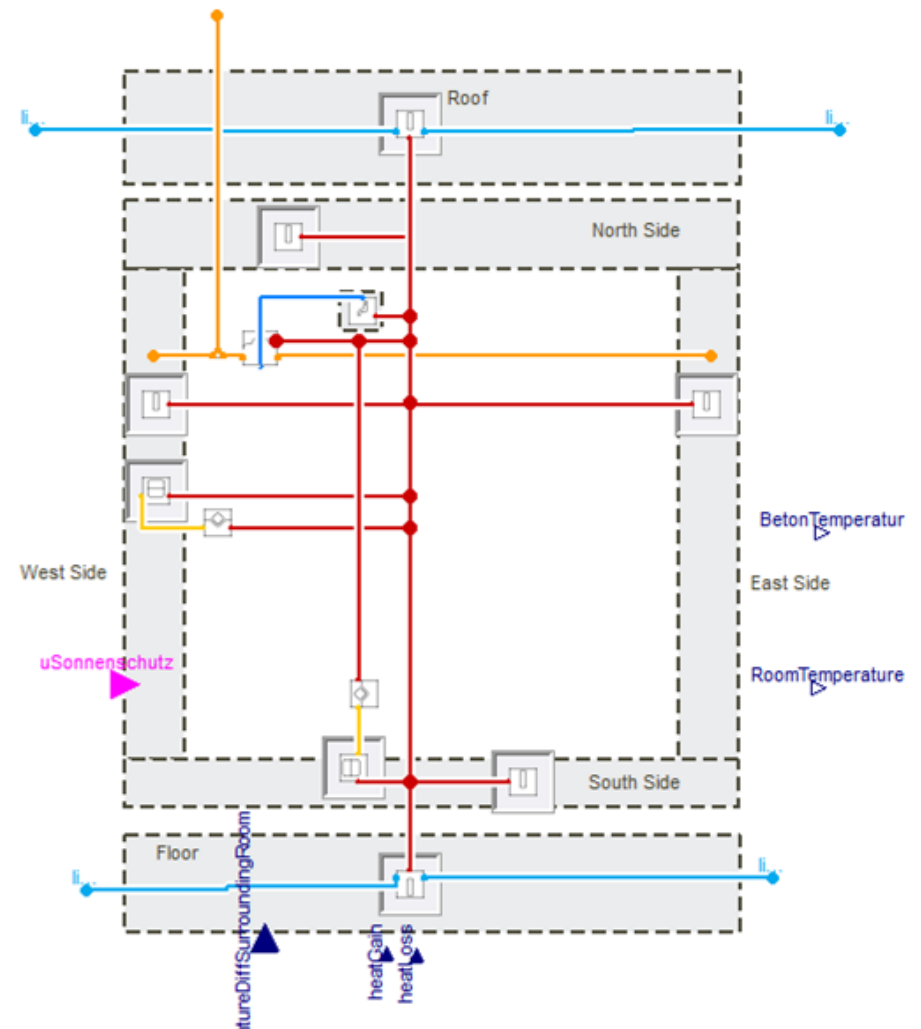
*Control input*

Compressor speed



# Modell of Building – Thermoactive Ceiling

- Temperature of room regulated with water between 15°C and 35°C
- Modelling of significant heatflows
- Model reduction leads to ODE with about 25 states



# Fluid Properties Calculation

- Many fluid properties (e.g. heat capacity) are discontinuous at saturation curve

New approach:

- Inputs:  $p$ ,  $h$
- Calculate superheated, subcooled  $h$ :

$$h^+ := h - h^{\text{vap}}(p)$$

$$h^- := h - h^{\text{liq}}(p)$$

- Coordinate transformation

$$(p, h) \rightarrow \begin{cases} (p, h^+) & \text{if } h \geq h^{\text{vap}} \\ (p, h^-) & \text{if } h \leq h^{\text{liq}} \end{cases}$$

- Evaluate tabulated bicubic splines on transformed coordinates

